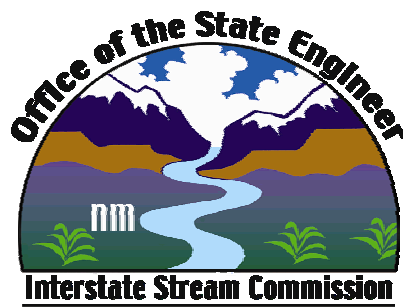


REVISED MODEL OF THE TULAROSA BASIN



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Revised Model of the Tularosa Basin

INTRODUCTION

A numerical model of the Tularosa Basin (Morrison, 1989) has been used to predict drawdown and administer the basin. The 1989 model is still well calibrated in much of the basin but new information warrants an update of the model. The model has been redesigned to include observed and estimated pumping through June 2005. There is also new water level and aquifer test data available to constrain the calibration.

Other modifications have been added. The wet season from 1975 to 1995 altered the model assumptions on recharge. Recharge along the Mountain front has been modified to reflect increased recharge during higher precipitation periods. Also, head dependant model cells were added to relate surface elevation and water elevation to evaporation losses.

The statistical fit by every calibration measure has been improved with the 2005 model. The revised model can be used to project 40-year drawdown using a projected growth rate for the basin.

BOUNDARIES AND MODEL STRUCTURE

The revised model is run in MODFLOW96 (Harbaugh and McDonald, 1996) in units of feet and days. Figure 1 shows the grid layout of the 2005 model. It is slightly larger than the 1989 model. The grids have the same eastern extent along the uplift of the Sacramento Mountains. The new grid extends ¼ mile further than the 1989 grid in the north, south and west directions. In the 2005 model, a cell size of 0.5 mile by 0.5 mile is universally applied.

As in the 1989 model, the grid orientation is rotated counterclockwise 15 degrees. The bottom-left corner of the revised grid is at

UTM X: 392,856 meters

UTM Y: 3,587,151 meters.

The Projected Coordinate System is NAD 1983, UTM Zone 13N.

The active portion of the model represents Basin Fill. As in the 1989 model, the east side of the active grid is along the Sacramento Mountain uplift. The Permian and Pennsylvanian through Precambrian rocks of the uplifted area are much less transmissive than in the Basin Fill as indicated by steeper water level gradients and wells with lower yields. From observation of water elevation contours and watershed delineation, most of the flow enters the active grid area along the eastern mountain front as runoff.

Boundaries to the north, south and west of the grid were conceptualized as no-flow.

These boundaries are also outside of the influence of most historical pumping. As distance from the mountain front increases, the Basin Fill is generally composed of finer grained, less permeable material.

As in the 1989 model, the Basin Fill is represented as an unconfined aquifer with a single transmissivity layer. In reality, the Basin Fill is of variable depth forming a trench thousands of feet deep and underlain by Permian rocks of unknown permeability. Most of the wells and available pump tests partially penetrate the Basin Fill. The water at depth, in general, is more saline, although a USBR (2003) borehole at Township 16S, Range 9E, Section 36 found a total dissolved solids inversion of 5200 ppm to 1100 ppm at depths from 645 to 1240 feet below ground surface. Information on how parameters for vertical and horizontal conductance, storage and salinity change with depth is limited. Selection of parameters for a multi-layer model would be largely guesswork with very little information to constrain it. For these reasons, a reasonable calibration was achieved with as simple of a model as possible.

RECHARGE

No direct aerial recharge was simulated in the model. The basin precipitation of 12 inches/year is much less than the evaporation of 72 inches/year.

Simulated mountain front recharge was placed at the watershed / basin fill intersection cells as shown in figure 2. Watersheds with an area of greater than 4000 acres were delineated in the Sacramento Mountains. Precipitation falling in each watershed was estimated by using a linear relationship to correlate observed precipitation to surface elevation at nearby gages. Figure 3 shows the relationship in the area to be

$$\text{Annual Precipitation (in/yr)} = 0.0038 * \text{Surface Elevation (ft msl)} - 6.51$$

Initially, the total recharge rate from the 1989 model of 14,847 AFY was proportioned to watershed rainfall portion in each of the 22 watersheds. In the calibration of the 2005 model, watersheds 1 through 15 were the primary contributors of recharge. Watershed 16 contributed recharge only in high precipitation periods and recharge from watersheds 17 through 22 were deleted. This decreased the total recharge to 11,890 AFY.

The areas for watersheds 1 through 15 were multiplied by the precipitation at the centroid of the watershed to obtain the total volumetric rate of rainfall. This rate is 539,593 AFY. The watershed delineation and precipitation calculation differ from the 1989 model. The simulated mountain front recharge of 11,890 AFY is 2.2% of the available precipitation. This percentage differs from the 1989 model that delivered 2.7% of precipitation as mountain front recharge. Table 1 shows the recharge calculation.

The 1989 model is not well calibrated to some wells near Tularosa between 1975 and 1995. Figure 4 shows that this was a high precipitation period and that there was a corresponding buildup in water elevations that is not simulated in the 1989 model. In calibration of the revised model, the recharge was stepped up to 26,983 AFY for the high precipitation period then stepped back down to a rate of 11,890 AFY. Figure 5 shows the observed Rio Tularosa discharge near Bent and the simulated mountain front recharge. Proportionally, mountain front recharge approximates the increased rise in discharge on the Rio Tularosa. Additional mountain front recharge was applied to the model during

this period along additional lengths of drainages. The locations of the additional recharge cells were shown in figure 2. Each additional recharge cell has a specified flux of 150,000 cfd (1258 AFY). The number of additional recharge cells along drainages was largely a factor of calibration to observed water level mounding rather than size or elevation of a source watershed.

DISCHARGE

In the 1989 model evapotranspiration was represented in the model with specified fluxes. In the revised model, the rate of evaporative discharge is related to the simulated depth to water. This was done using the MODFLOW evaporation package. The land surface elevations from a 30-meter digital elevation model (DEM) were digitized to the centers of the model cells. A maximum evaporation rate of 72 inches a year and an extinction depth of 20 feet were used.

It was possible to calibrate the model with a range of evaporation extinction depths. With an extinction depth of 6 feet, calibrated transmissivity in the model increases by about 40%. Typically, an extinction depth of 6 feet would be selected for barren soil, while 20 feet would be selected in a phreatophyte-covered area. Much of the surface area on the active model grid has very little phreatophyte activity. However, observed depths to water and LANDSAT imagery indicate that much of the evaporation occurs along phreatophyte-covered drainages.

John Shomaker and Associates, Inc. (2003) compiled historical pumping through 1999. The compilation was similar to the Morrison compilation to 1984 but JSAI added pumping outside of the administrative area, particularly north of Temporal Creek. The updated pumping compilation used municipal records for Alamogordo and Tularosa. It also contains the complete Holloman Air Force Base pumping that was initially compiled by JSAI for the water plan of the basin. JSAI updated the irrigation pumping with water rights files from the OSE office and cross-referenced this by doing a field survey. Reports by the USDA and NMASS and Wilson were also utilized. Because water elevation data was available after 1999, the simulation was extended through June 2005 with estimates of pumping based on projections of the 1999 pumping. Table 2 summarizes the pumping used in the model. No return flow was used in the revised OSE model.

MODEL CALIBRATION

The model was started from a predevelopment steady state simulation at 1/1/1910. A transient simulation was calibrated from 1/1/1910 to 6/30/2005.

Steady state and transient simulations were examined in conjunction to find the best statistical and visual fit to water level observations.

Initially, the single transmissivity and single storage that fit calibration points the best was determined. A transmissivity of 900 ft²/day and storage of 8% yielded the best calibration fit when a *single value* for transmissivity was used on the entire model grid. After the distribution of additional recharge cells in high recharge years was determined,

only transmissivity zones were delineated and varied to improve upon the calibration. Transmissivity calibration was guided by observed values of transmissivity.

Figure 6 shows the calibrated transmissivity zones and aquifer test observation points. This calibrated and observed transmissivity information is also tabulated in table 3. The aquifer test points aided in the delineation of the model transmissivity zones. Being a regional model, site-specific information does not always match the simulated parameters. Transmissivity zones were also delineated along river drainages and conceptual geology. The transmissivity of the aquifer is highest along river drainages and decreases as the thickness of the basin fill pinches out to the west. Storage of 8% was universally applied in the model.

The average value of transmissivity, $900 \text{ ft}^2/\text{day}$, was used in areas of the model where the model could have been calibrated with a wide range of transmissivity and either no aquifer test was available or multiple aquifer test results were highly variable.

STEADY STATE SIMULATION

In the steady state simulation, the only outflow of water in the model is at head dependant evaporation cells. Mountain front recharge enters the model at a rate of 11,890 AFY and exits via evaporation at a rate of 11,888 AFY. Model convergence error accounts for the other 2 AFY. The model iterates to determine the discharge and location of the model evaporation cells. The distribution of steady state evaporative outflow is shown in figure 7. The largest outflow model cells are along drainages. The simulated areas of outflow correspond with areas of observed shallow depth to groundwater.

A steady state water elevation set was constructed from wells with early measurement data and wells at a great distance from pumping effects. Water elevation contours for the steady state simulation and residuals for the steady state calibration wells are shown in figure 8. Observed and computed steady state water elevations and residuals are also summarized in table 4. In most areas of the model, residual errors are scattered in a non-systematic or random manner. The scatter is shown in figure 9 along with the idealized perfect fit line. Table 5 shows the steady state summary statistics for the 2005 model, the one-transmissivity model and the 1989 model. Steady state statistics have been improved with the 2005 model.

TRANSIENT SIMULATION

Drawdown and buildup contours from steady state through June 2005 are shown in figure 10. Three Rivers and the area 9 miles north of Tularosa still show residual mounding due to the high recharge period from the years 1975 to 1995.

A set of 393 wells and 2073 observed data points of well water elevations from USGS hydrograph data and field measurements from JSAI and the OSE was used in the transient calibration. The water elevation data set spans from January 1911 to March 2004. A subset of 17 wells was selected to graphically compare observed to simulated water elevations throughout the model area.

Figure 10 also shows the locations of these 17 hydrographs dispersed about the model area. Figure 11 compares observed and simulated water elevations at these locations. The simulated water elevations are shown for the 1989 and 2005 models. Pumping was updated in the 1989 model. The 2005 model achieves a better calibration in the northern portion of the model. Observed rises in hydrographs, particularly in the Tularosa area, were due primarily to an increase in mountain front recharge. This increased recharge was not simulated in the 1989 model.

The budget at the end of the calibration period is shown in table 6. Evaporative outflow at June 2005 is 9905 AFY. Decline in the water table due to groundwater pumping from pre-development steady state through June 2005, salvages 1983 AFY of evaporation. Figure 12 shows the annual simulated water budget from 1910 to June 2005.

Transient statistics for the 2005 model, the one-transmissivity model and the 1989 model are summarized in table 7. The statistical fit by every measure has been improved with the 2005 model. The transient residual mean has less bias. Residual standard deviation has been reduced to 31 feet.

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FIGURES

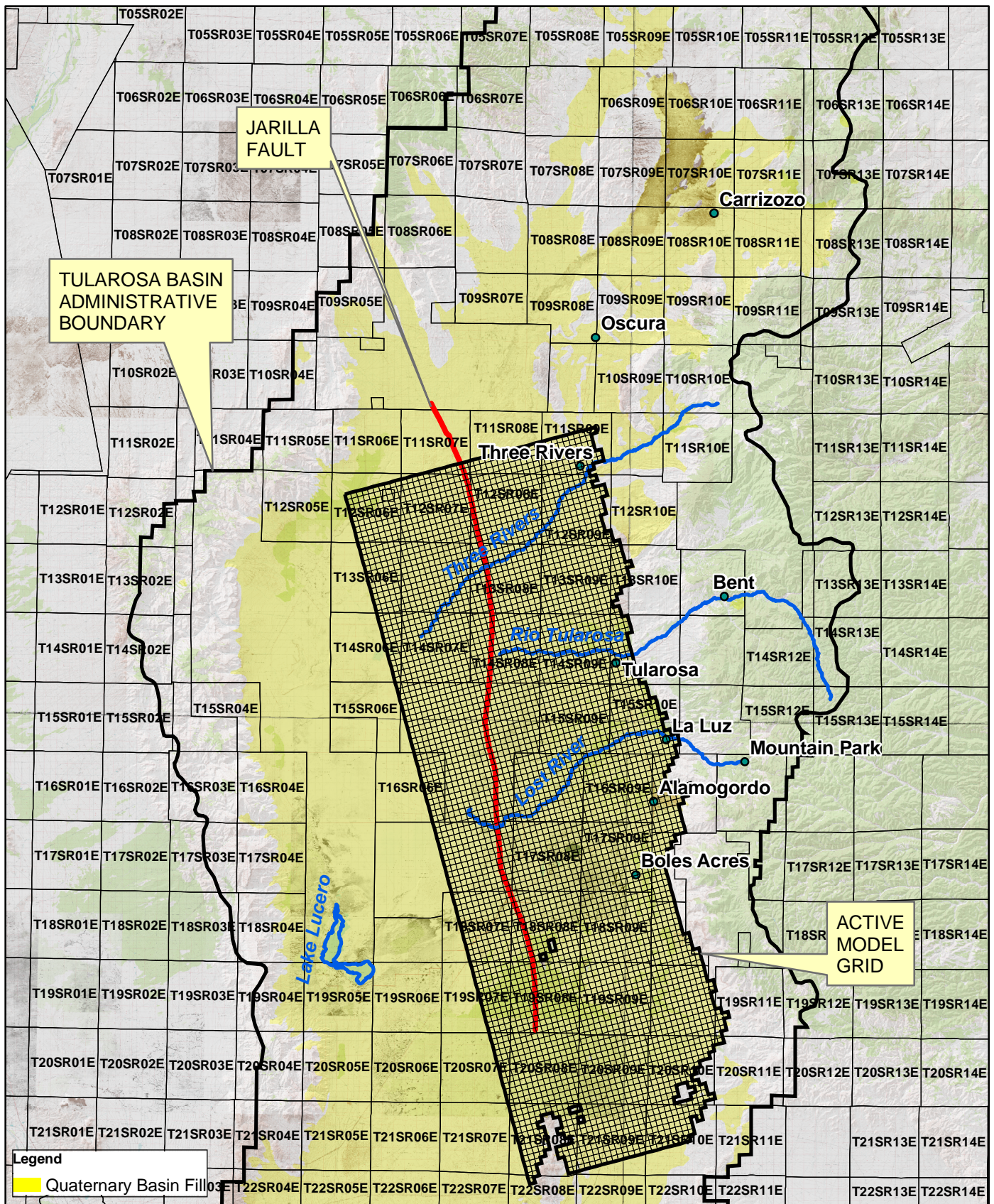


FIGURE 1
LOCATION MAP FOR THE ACTIVE MODEL GRID

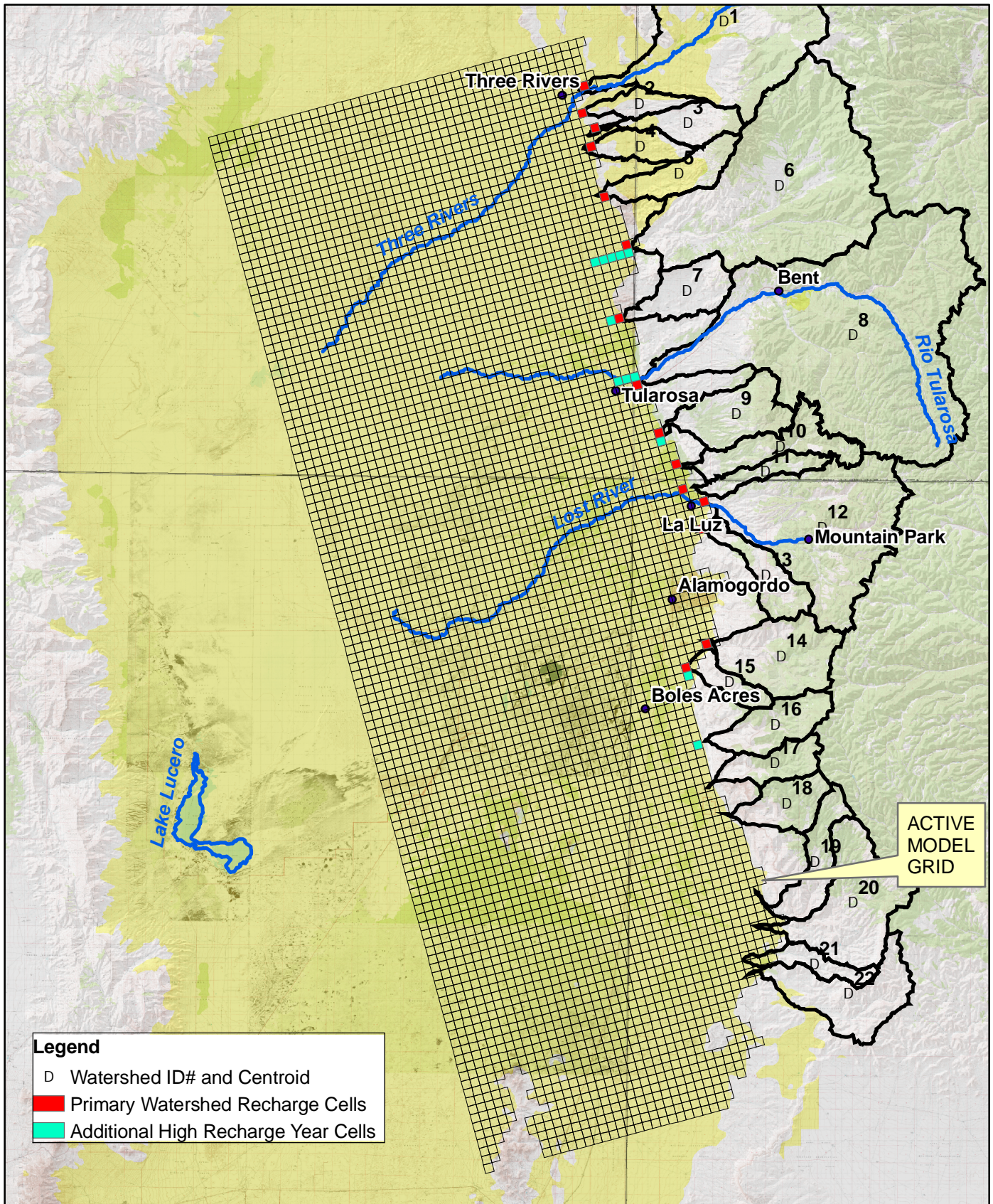
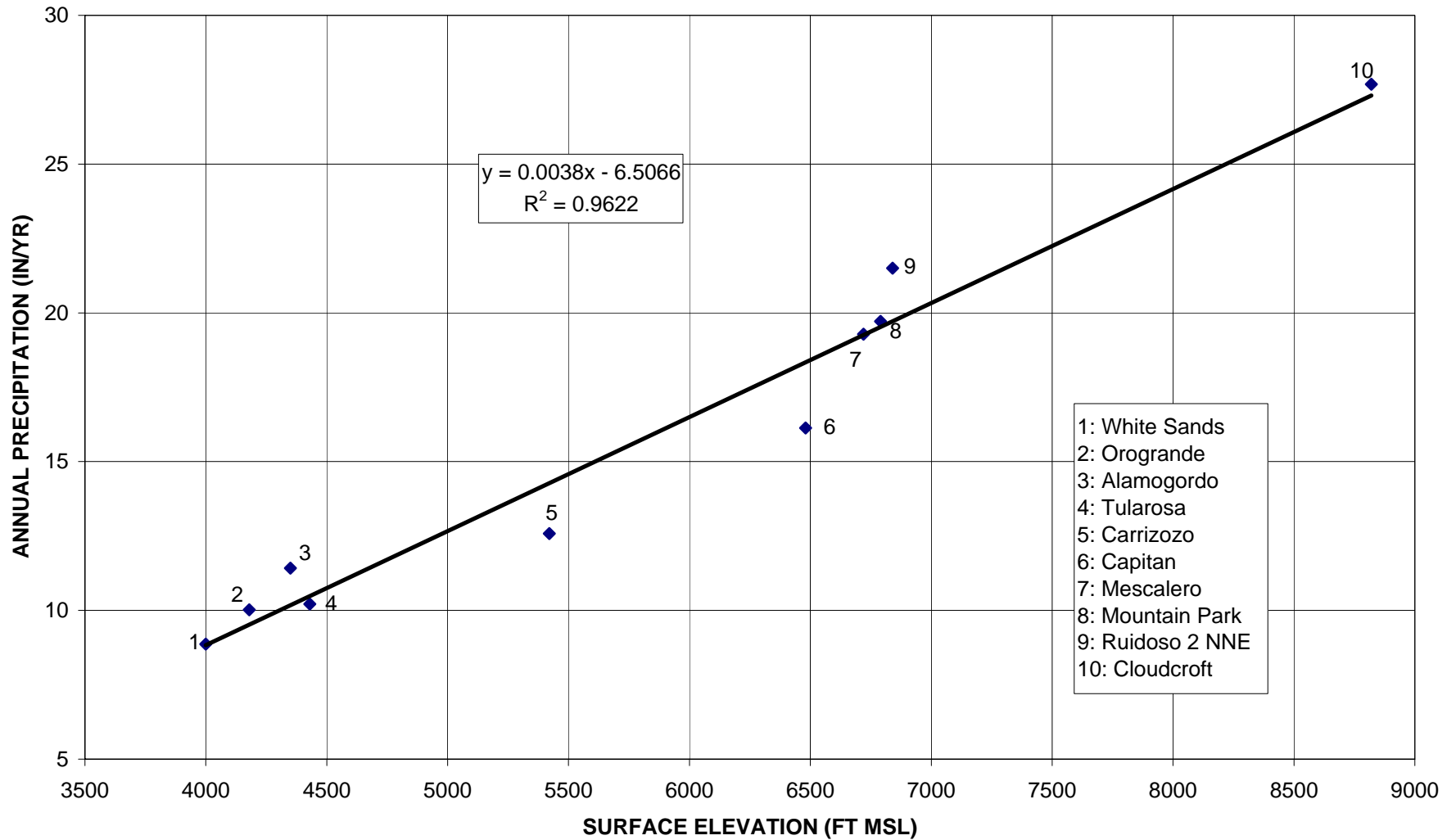


FIGURE 2
MOUNTAIN FRONT RECHARGE MODEL CELLS

FIGURE 3
VARIATION OF PRECIPITATION WITH SURFACE ELEVATION
AT GAGING STATIONS NEAR TULAROSA BASIN



**FIGURE 4
COMPARISON OF TULAROSA AREA DEPTH TO WATER
AND MOVING AVERAGE OF TULAROSA PRECIPITATION**

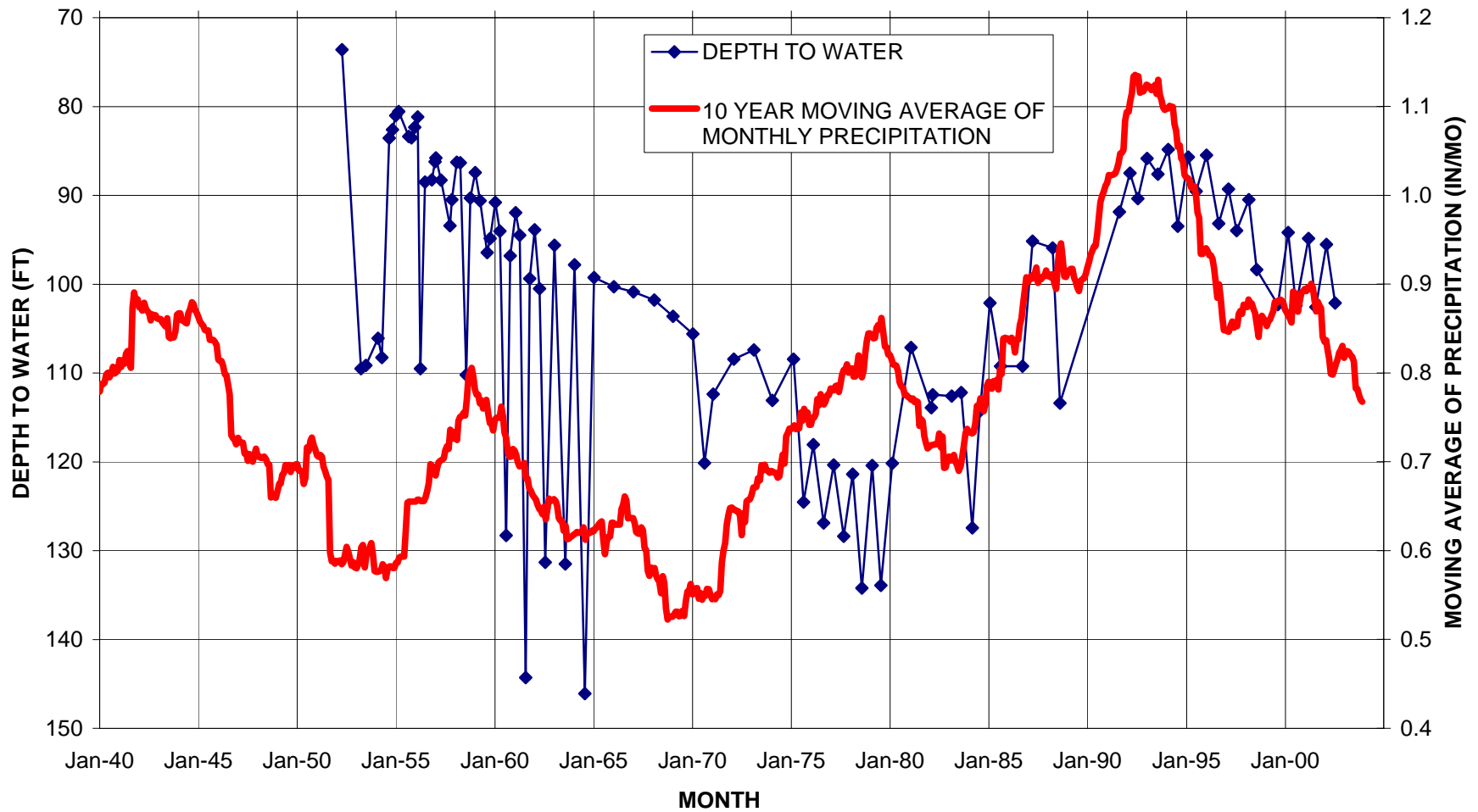
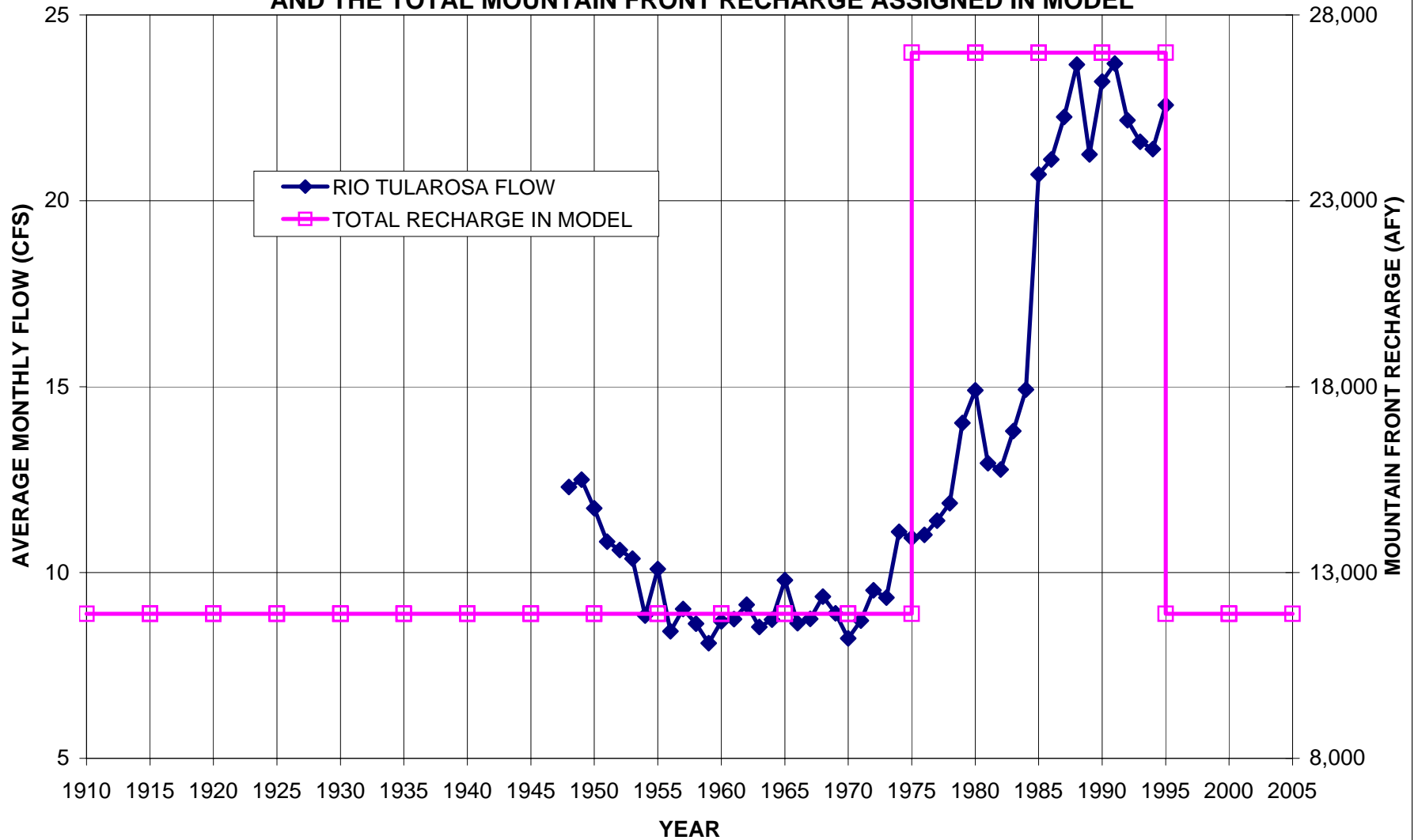
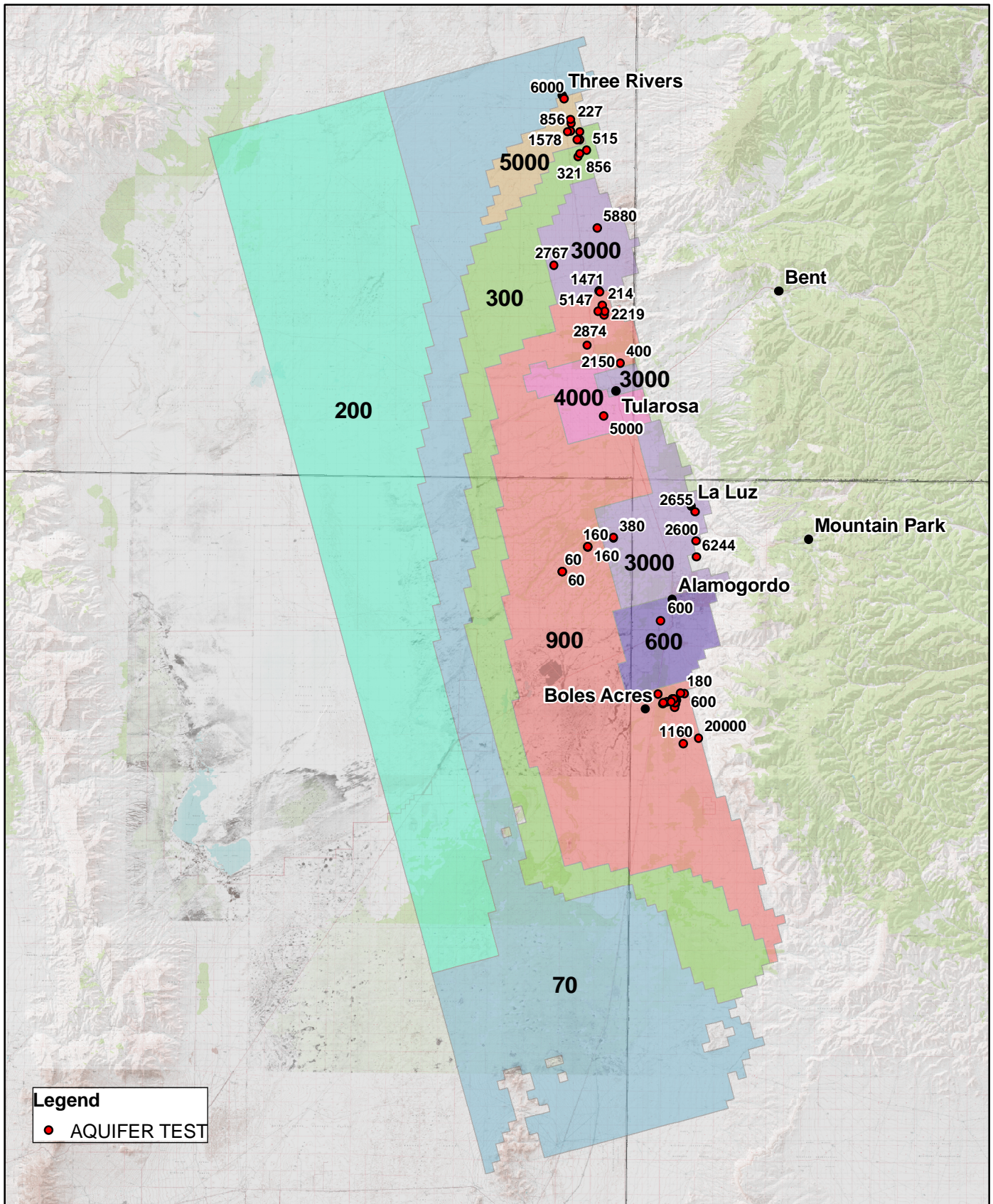


FIGURE 5
AVERAGE MONTHLY FLOW AT THE RIO TULAROSA GAGE NEAR BENT
AND THE TOTAL MOUNTAIN FRONT RECHARGE ASSIGNED IN MODEL



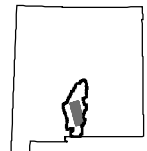


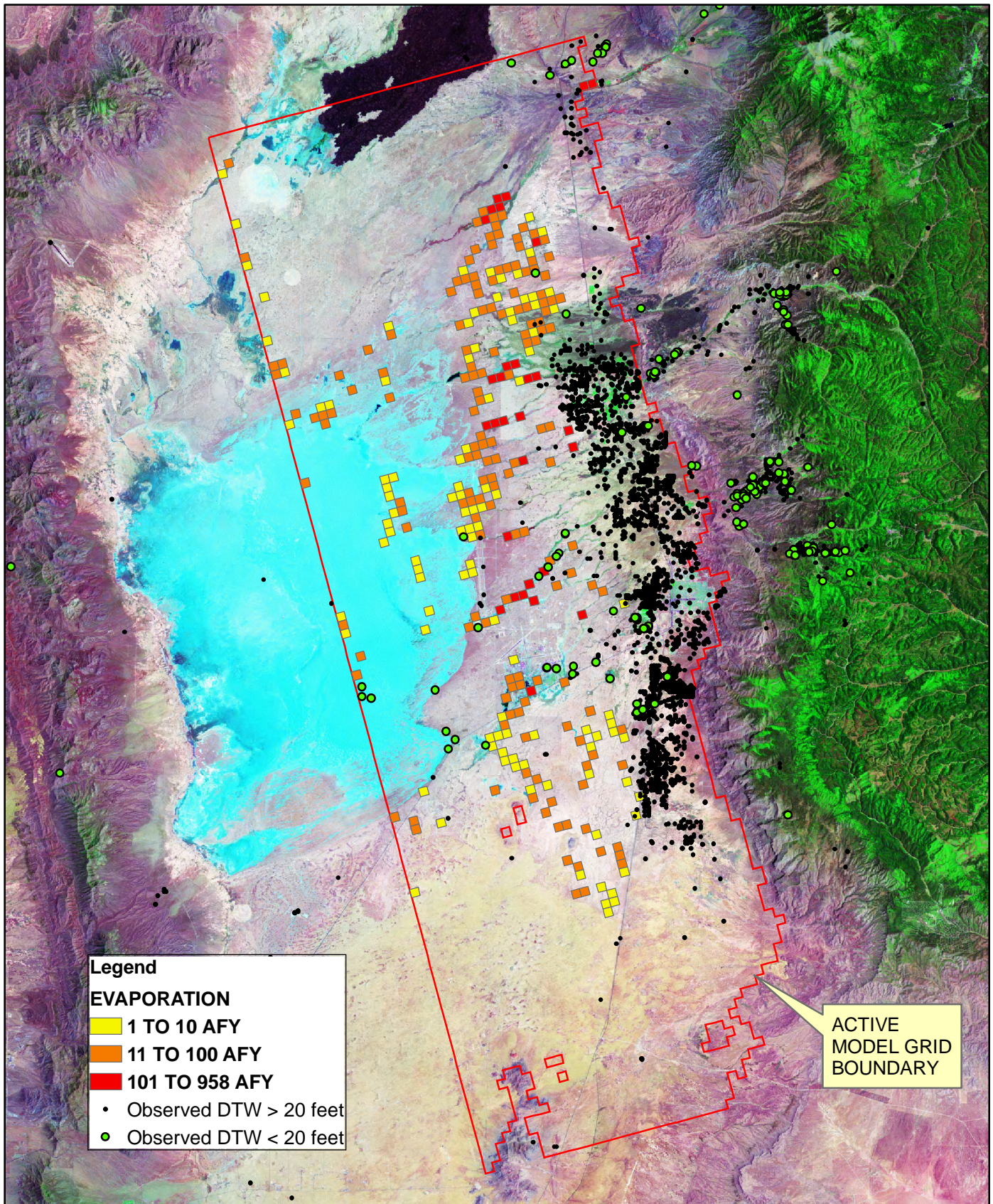
Legend
 ● AQUIFER TEST

0 4 8 16 Miles

TRANSMISSIVITY UNITS ARE IN FT²/DAY
 MODEL STORAGE IS UNIVERSALLY EQUAL TO 8%

FIGURE 6
 MODEL TRANSMISSIVITY
 WITH AQUIFER TEST POINTS OF TRANSMISSIVITY

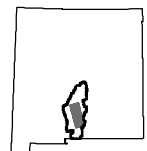


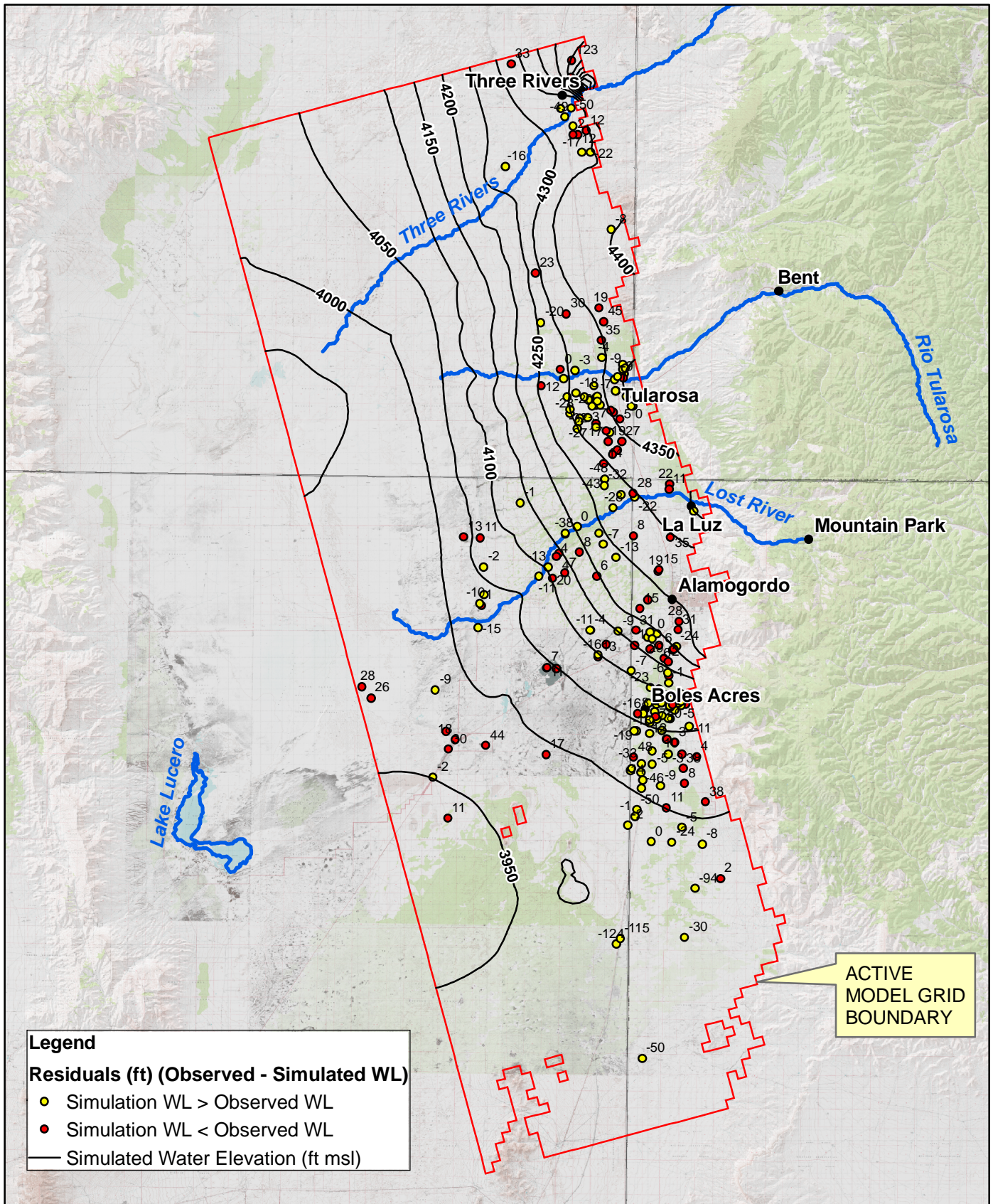


0 4 8 16 Miles

NASA Landsat Imagery (1995)

FIGURE 7
EVAPORATION LOCATIONS AND RATES
DETERMINED BY THE STEADY STATE MODEL





0 4 8 16 Miles

Contour Interval is 50-feet

FIGURE 8
OBSERVED - SIMULATED WATER ELEVATION RESIDUALS
AND SIMULATED STEADY STATE WATER ELEVATIONS

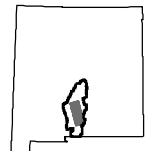
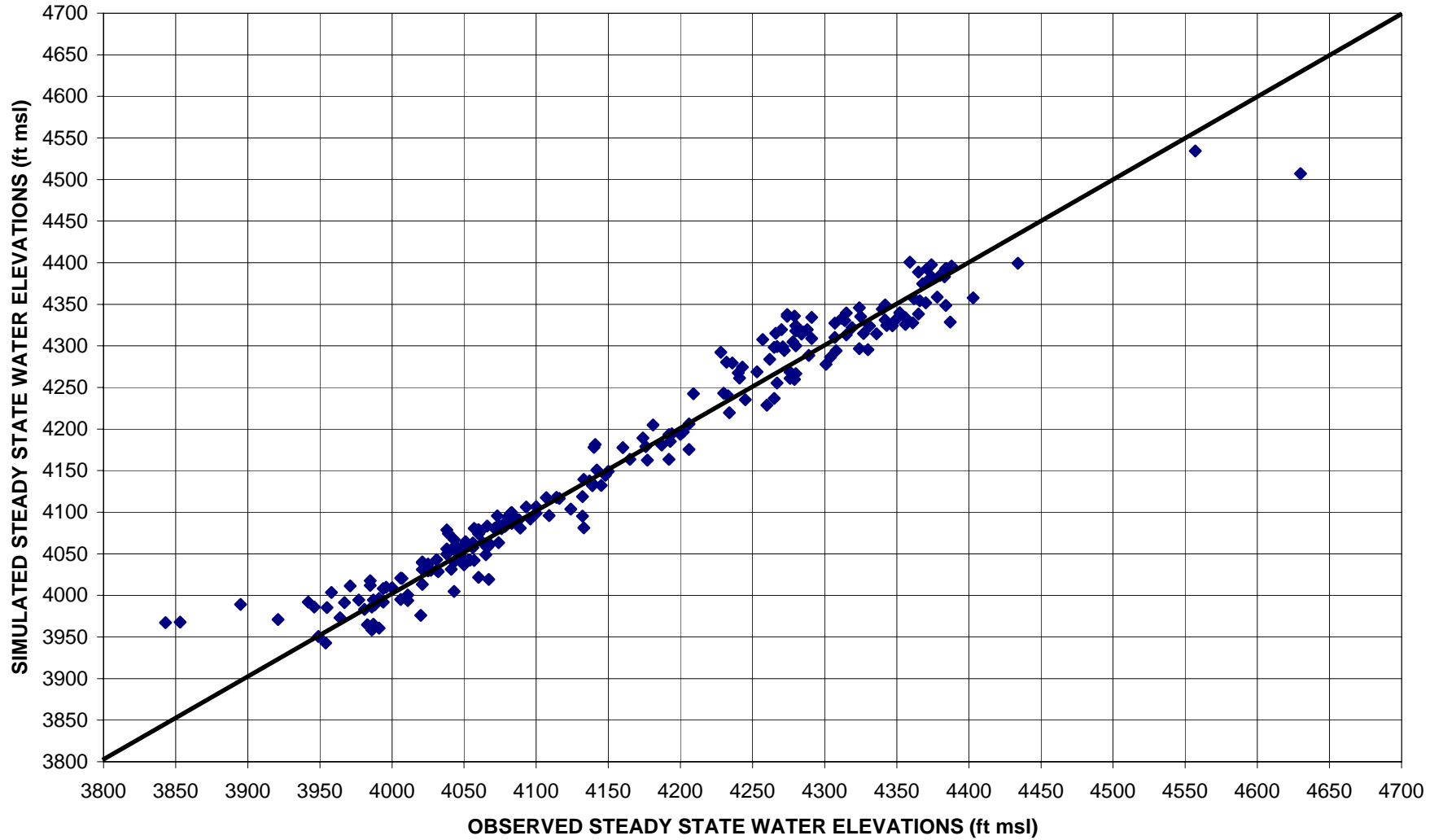


FIGURE 9
STEADY STATE COMPARISON OF OBSERVED WATER ELEVATIONS
TO SIMULATED WATER ELEVATIONS



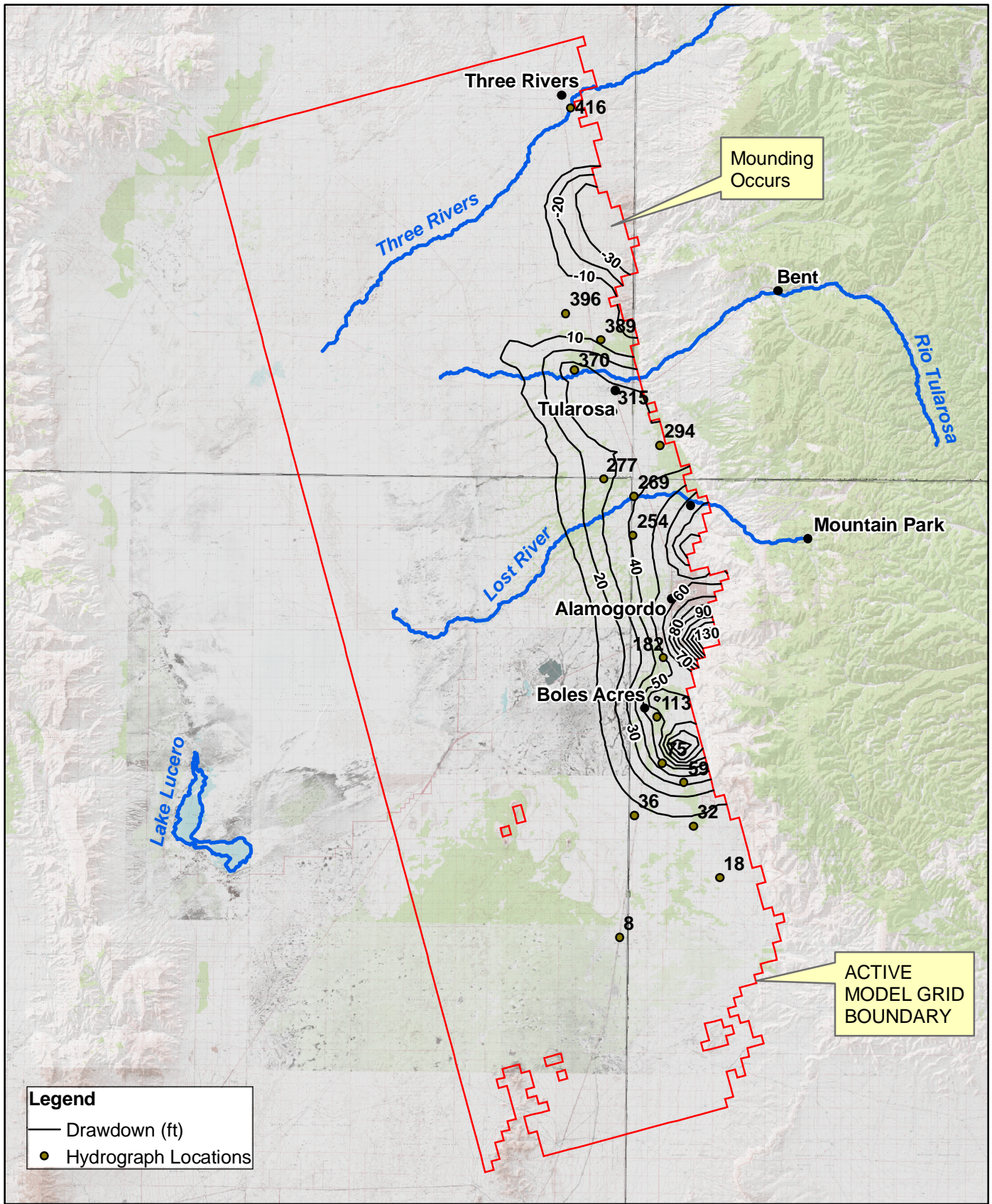
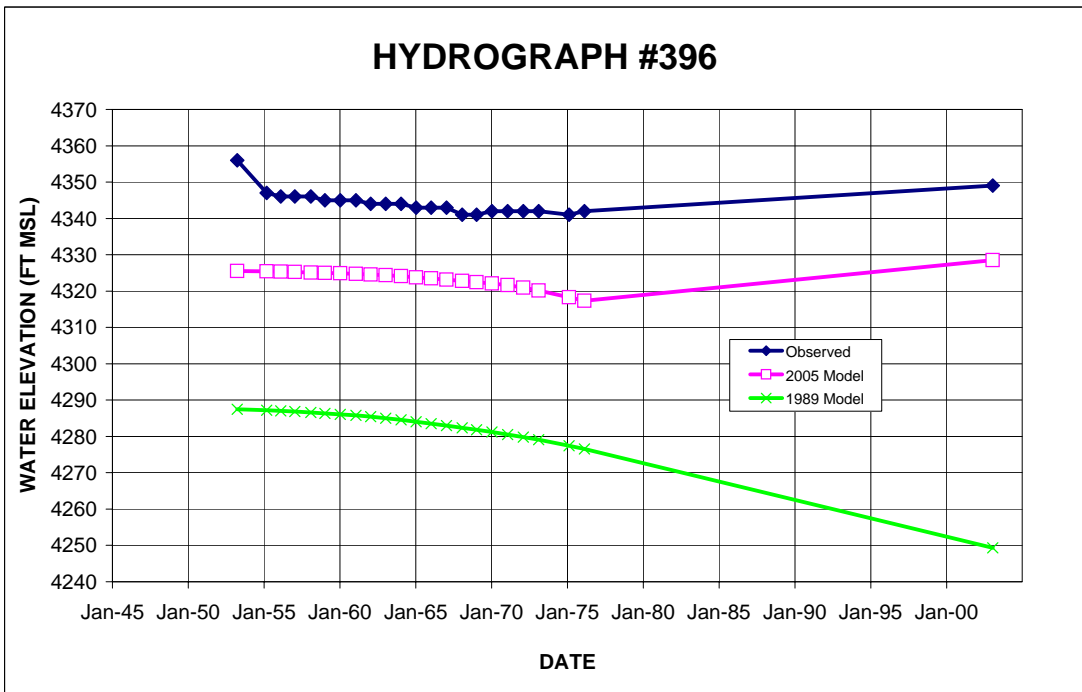
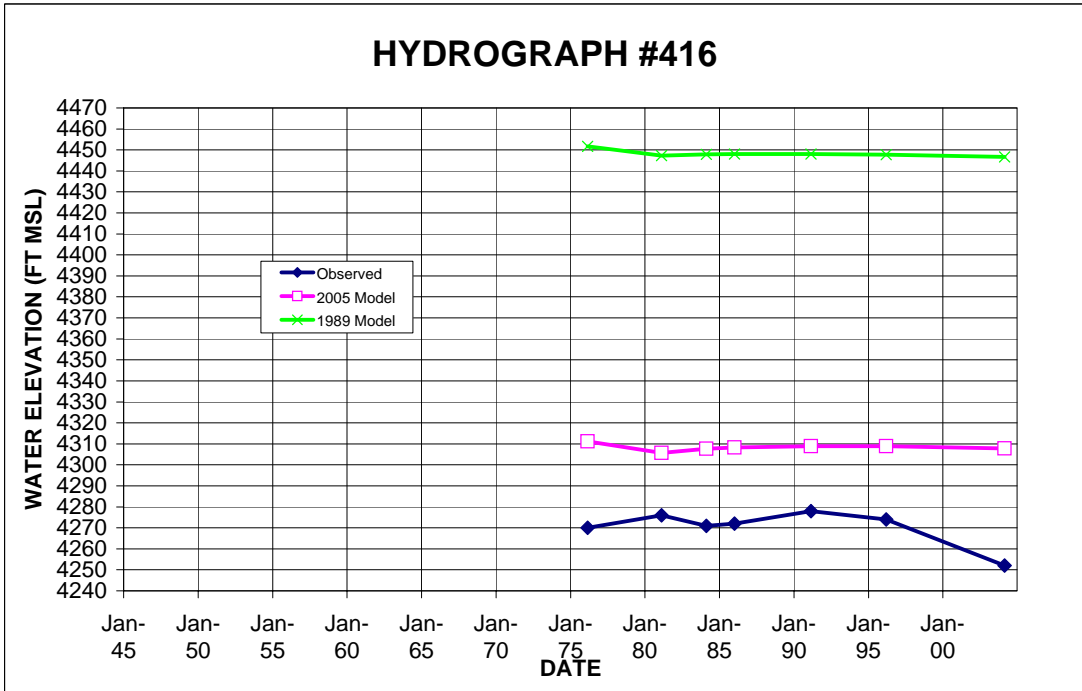
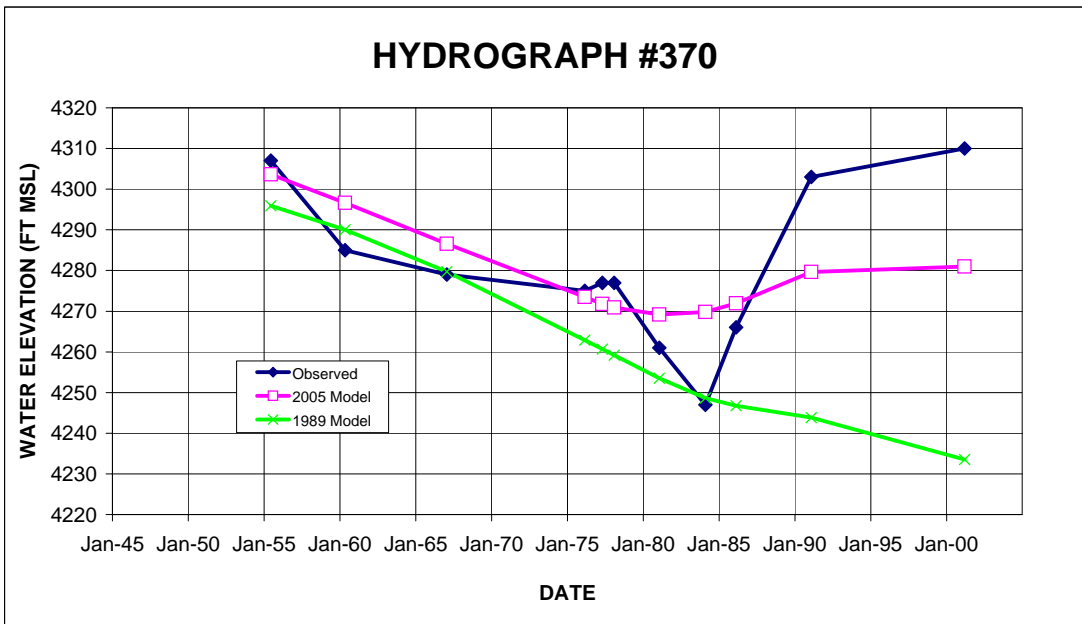
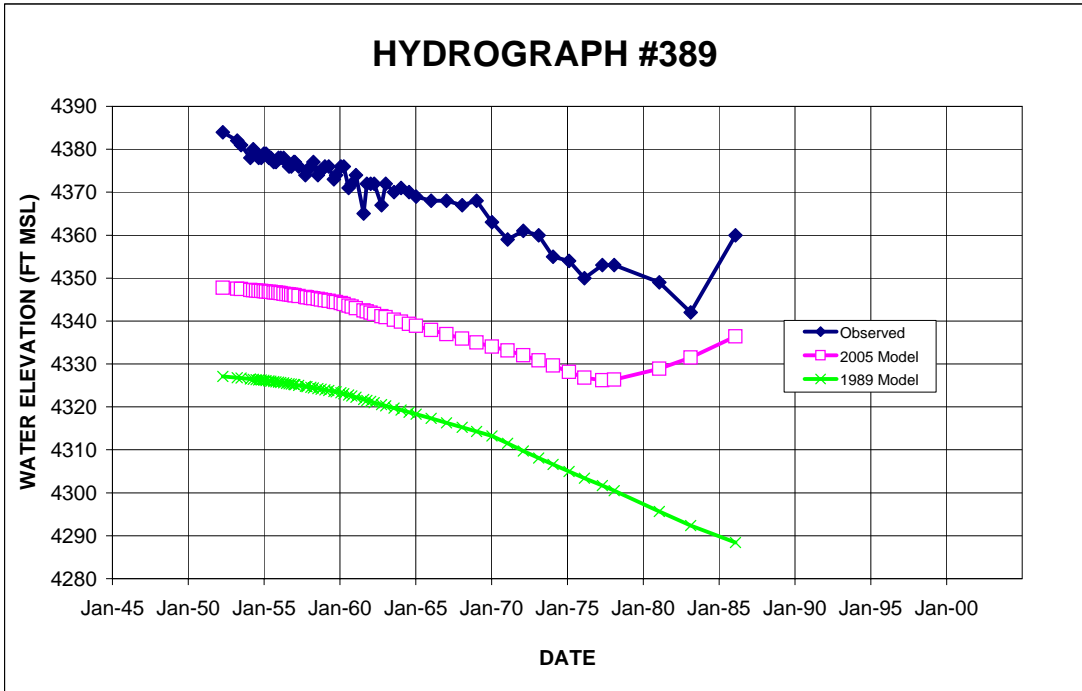


FIGURE 10
 SIMULATED DRAWDOWN FROM STEADY STATE TO JUNE 2005
 AND FIGURE 11 HYDROGRAPH LOCATIONS

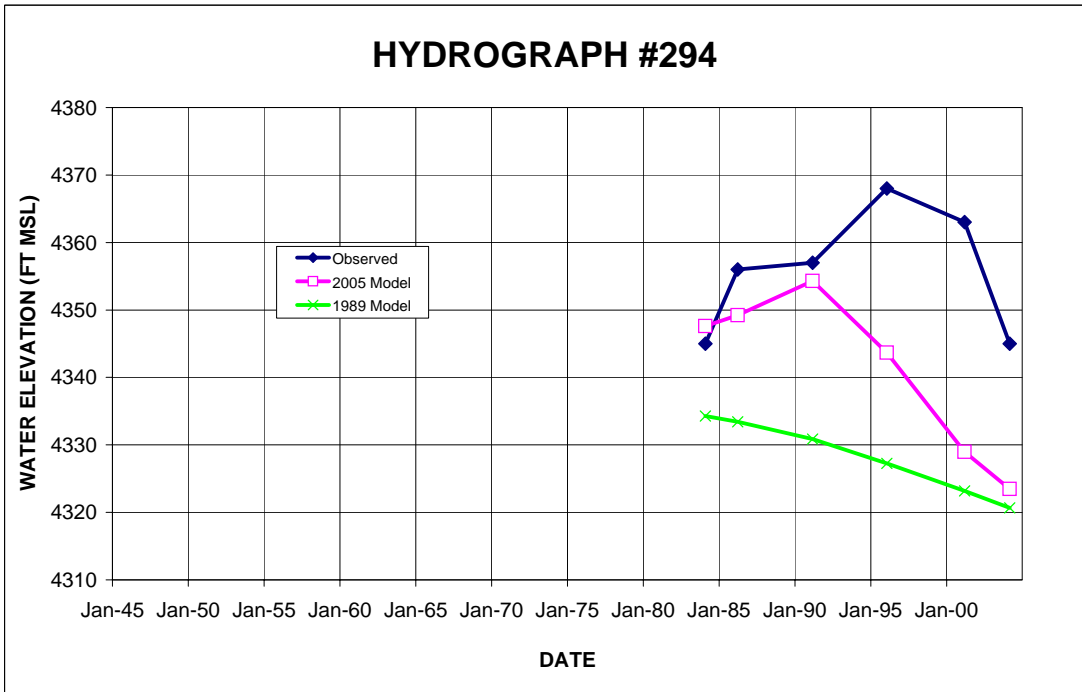
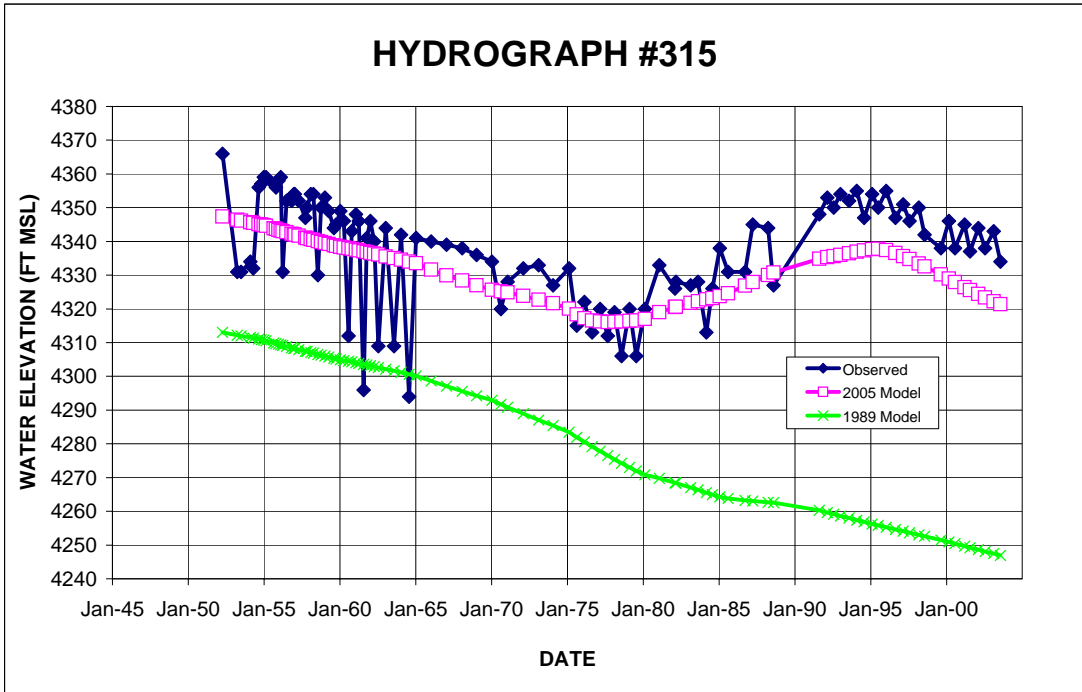
**FIGURE 11
COMPARISON OF SIMULATED TO OBSERVED HYDROGRAPHS**



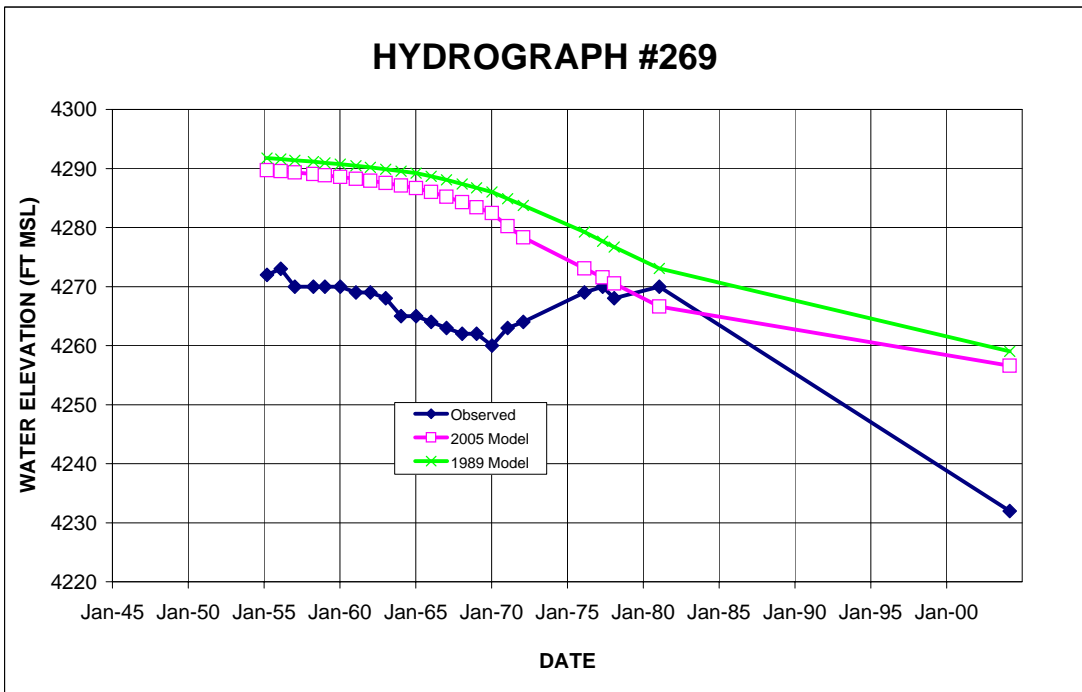
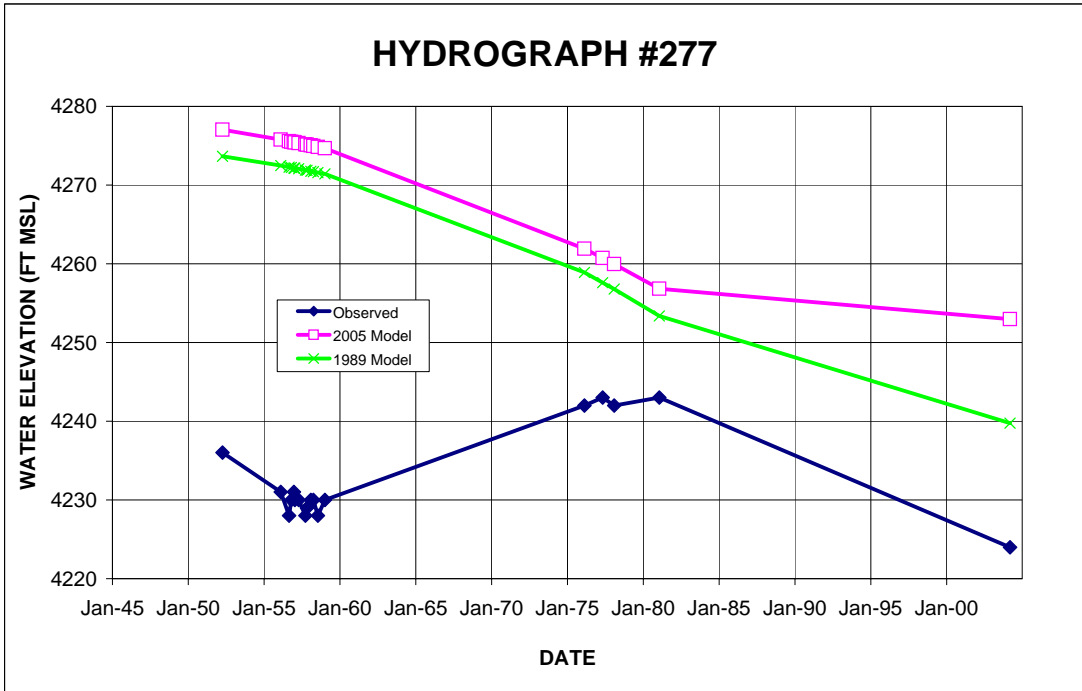
**FIGURE 11
COMPARISON OF SIMULATED TO OBSERVED HYDROGRAPHS**



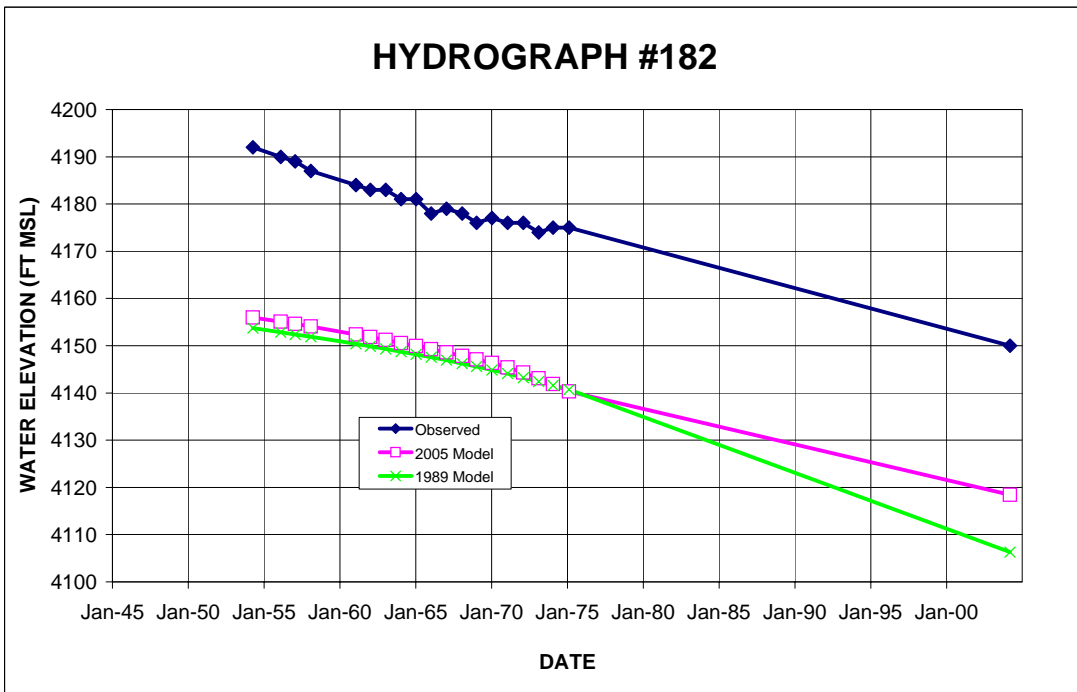
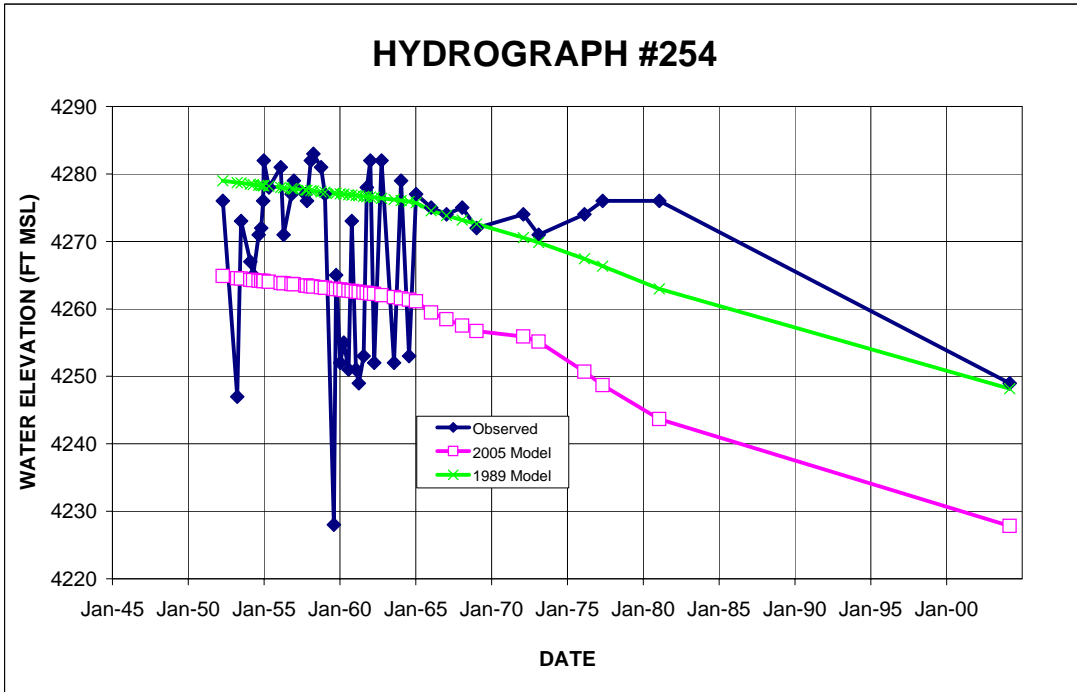
**FIGURE 11
COMPARISON OF SIMULATED TO OBSERVED HYDROGRAPHS**



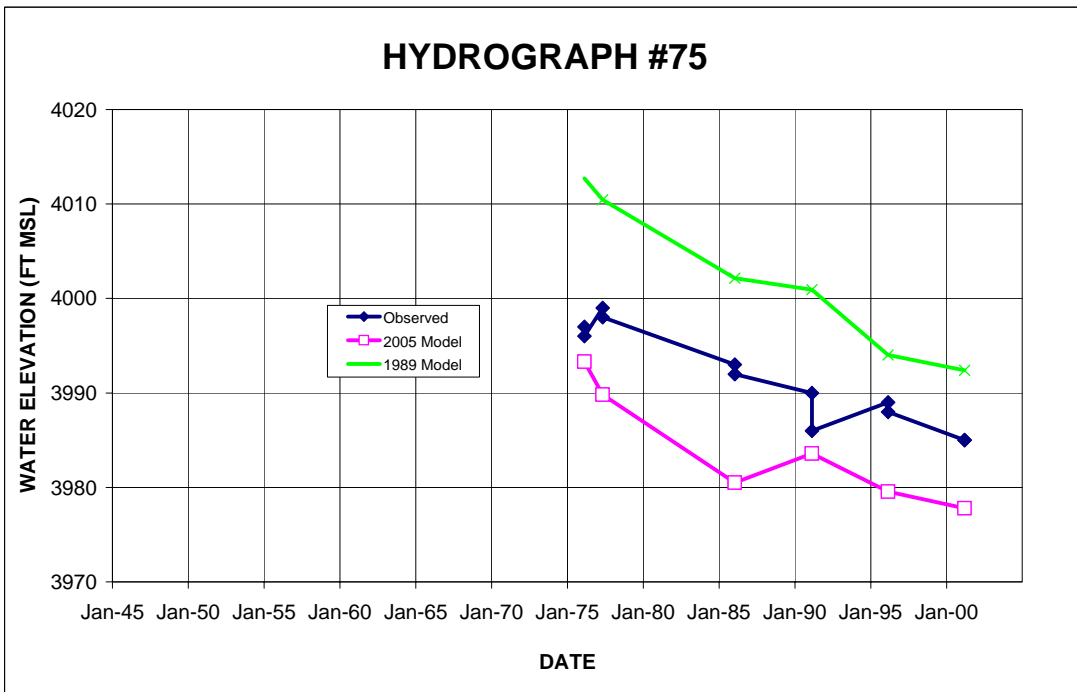
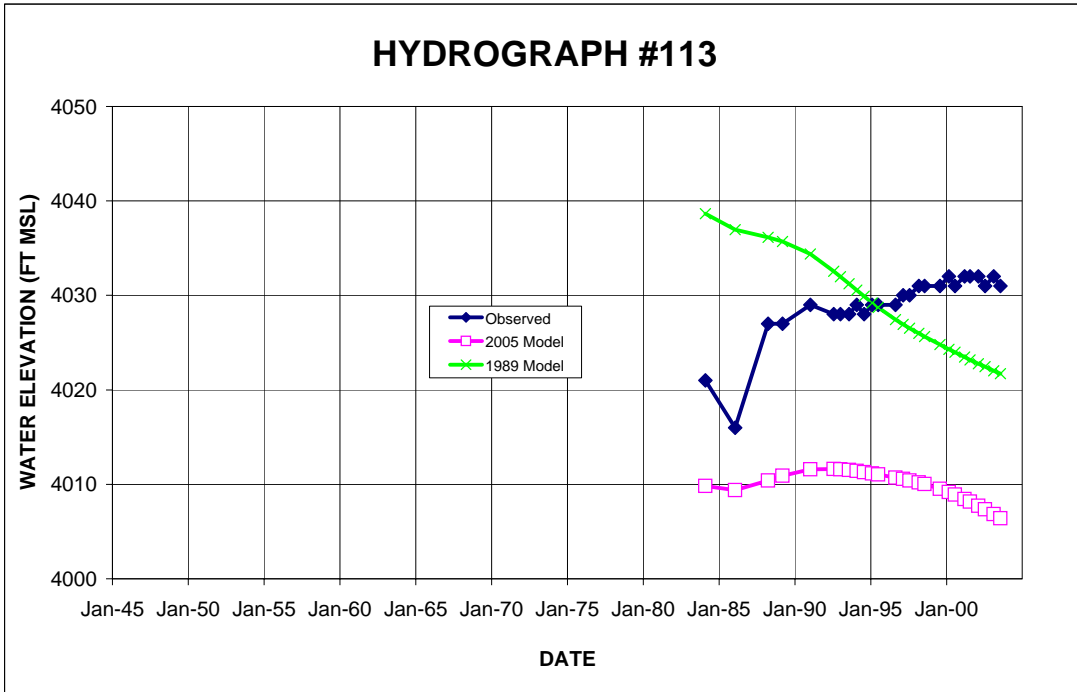
**FIGURE 11
COMPARISON OF SIMULATED TO OBSERVED HYDROGRAPHS**



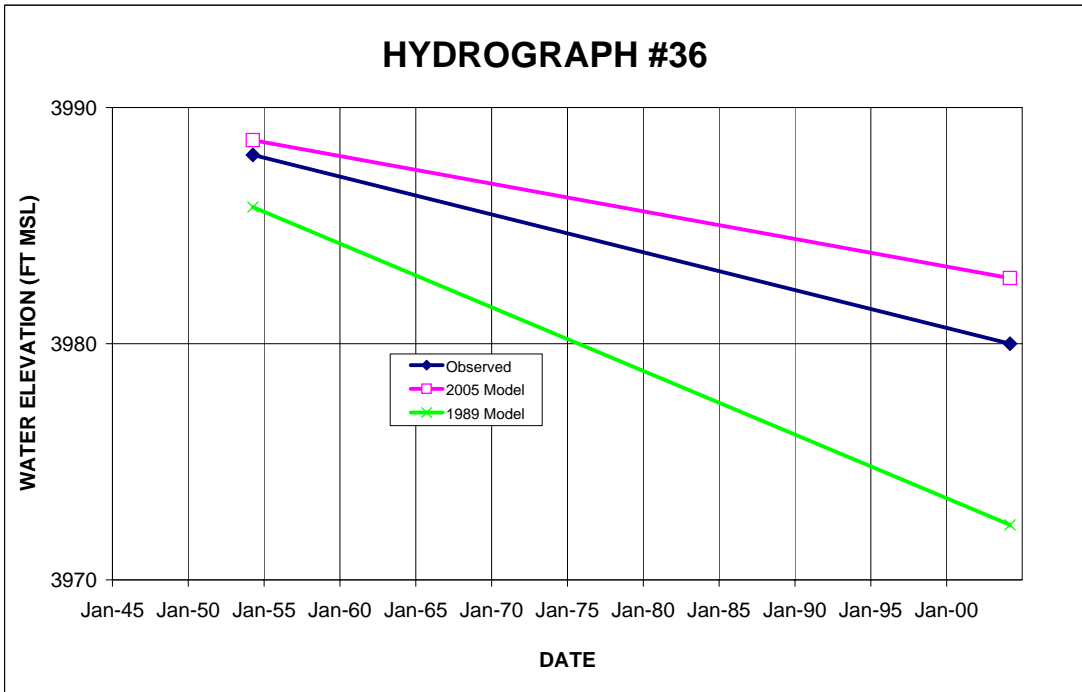
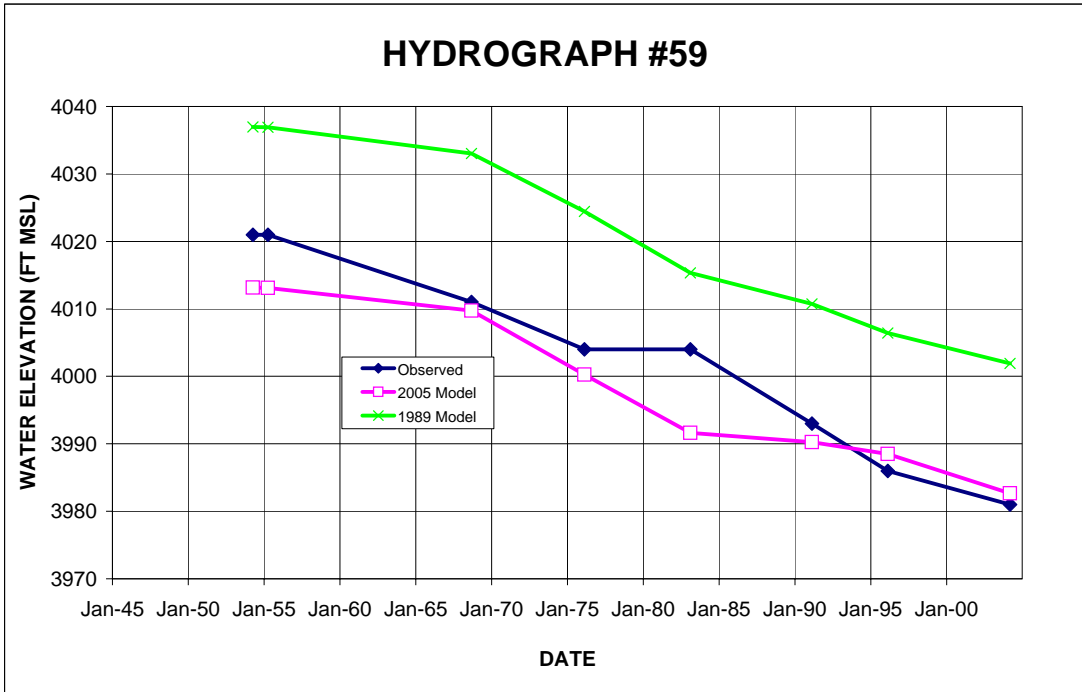
**FIGURE 11
COMPARISON OF SIMULATED TO OBSERVED HYDROGRAPHS**



**FIGURE 11
COMPARISON OF SIMULATED TO OBSERVED HYDROGRAPHS**



**FIGURE 11
COMPARISON OF SIMULATED TO OBSERVED HYDROGRAPHS**



**FIGURE 11
COMPARISON OF SIMULATED TO OBSERVED HYDROGRAPHS**

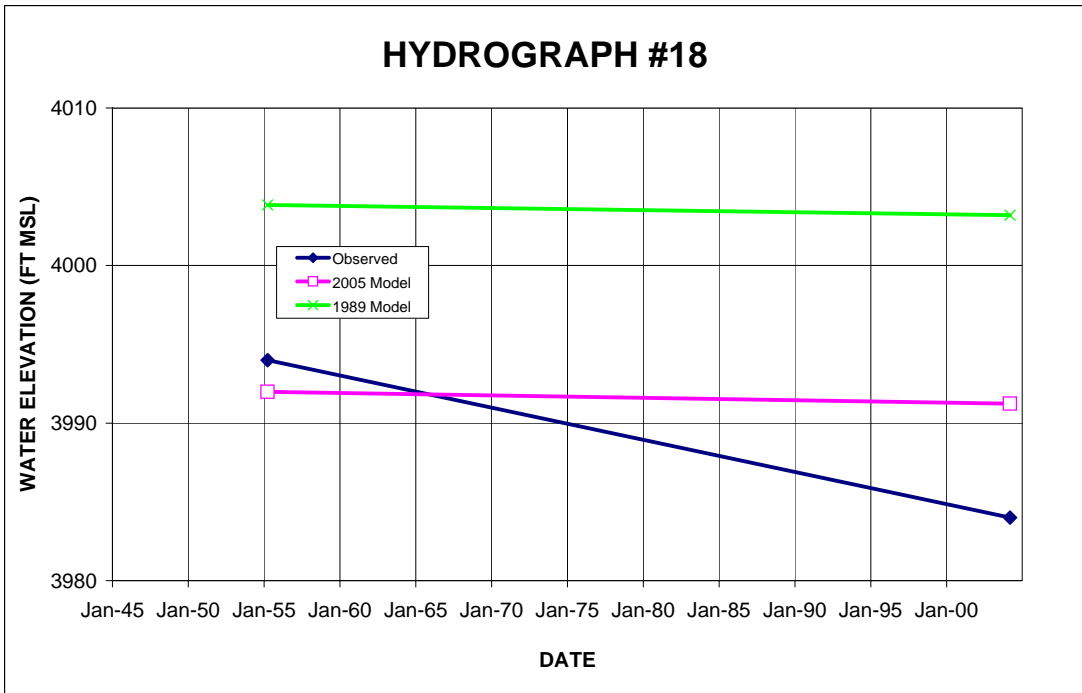
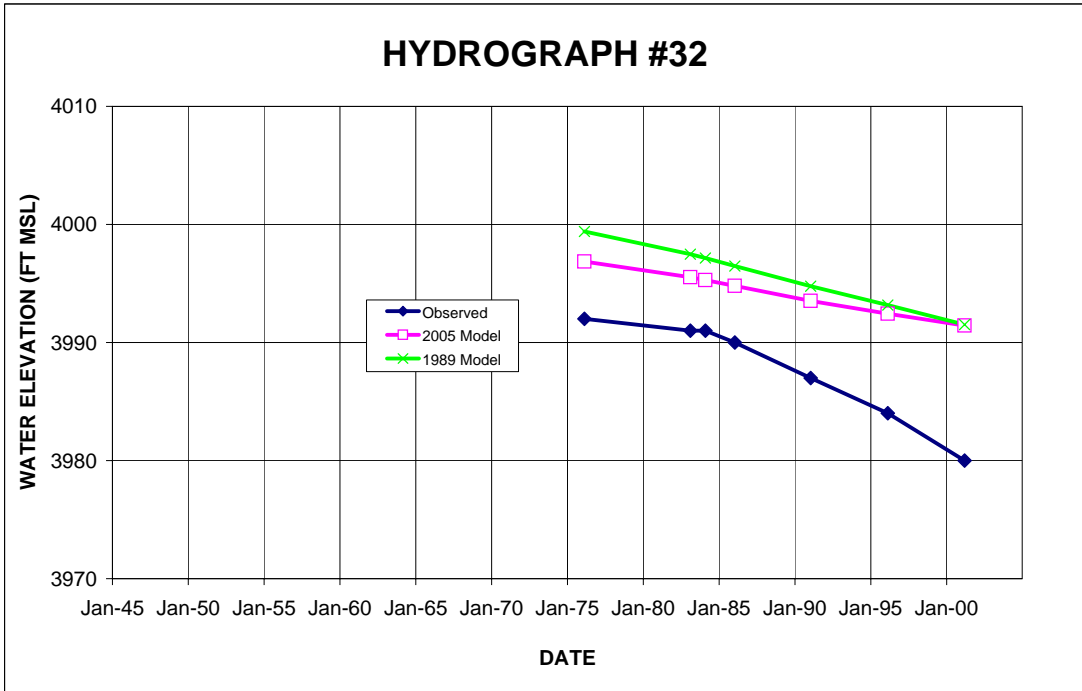
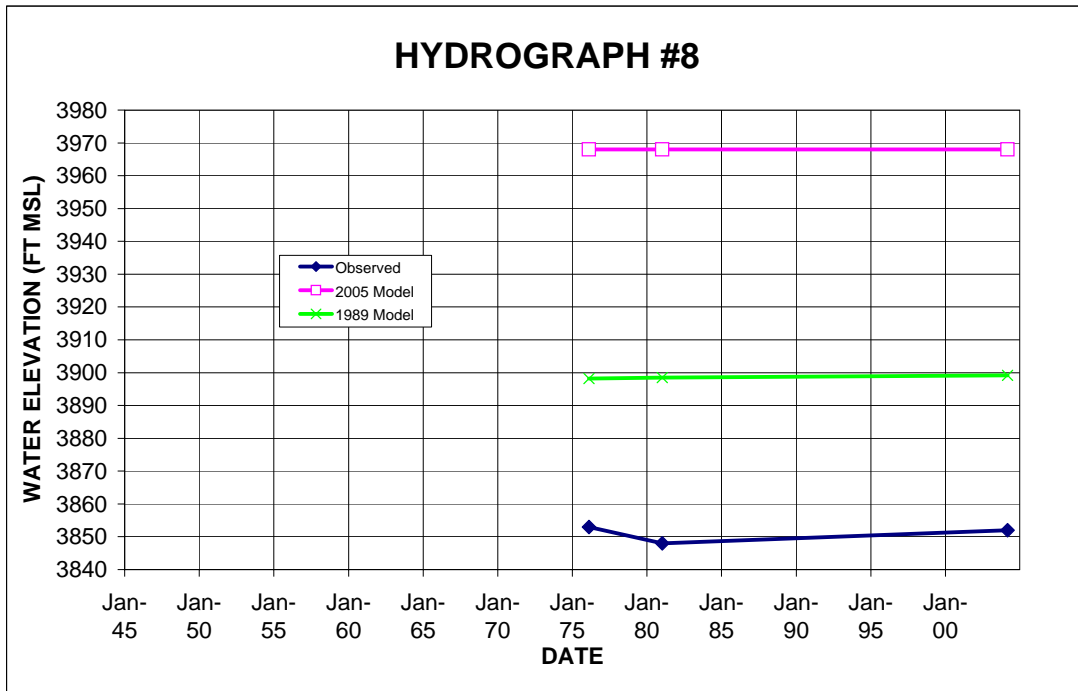
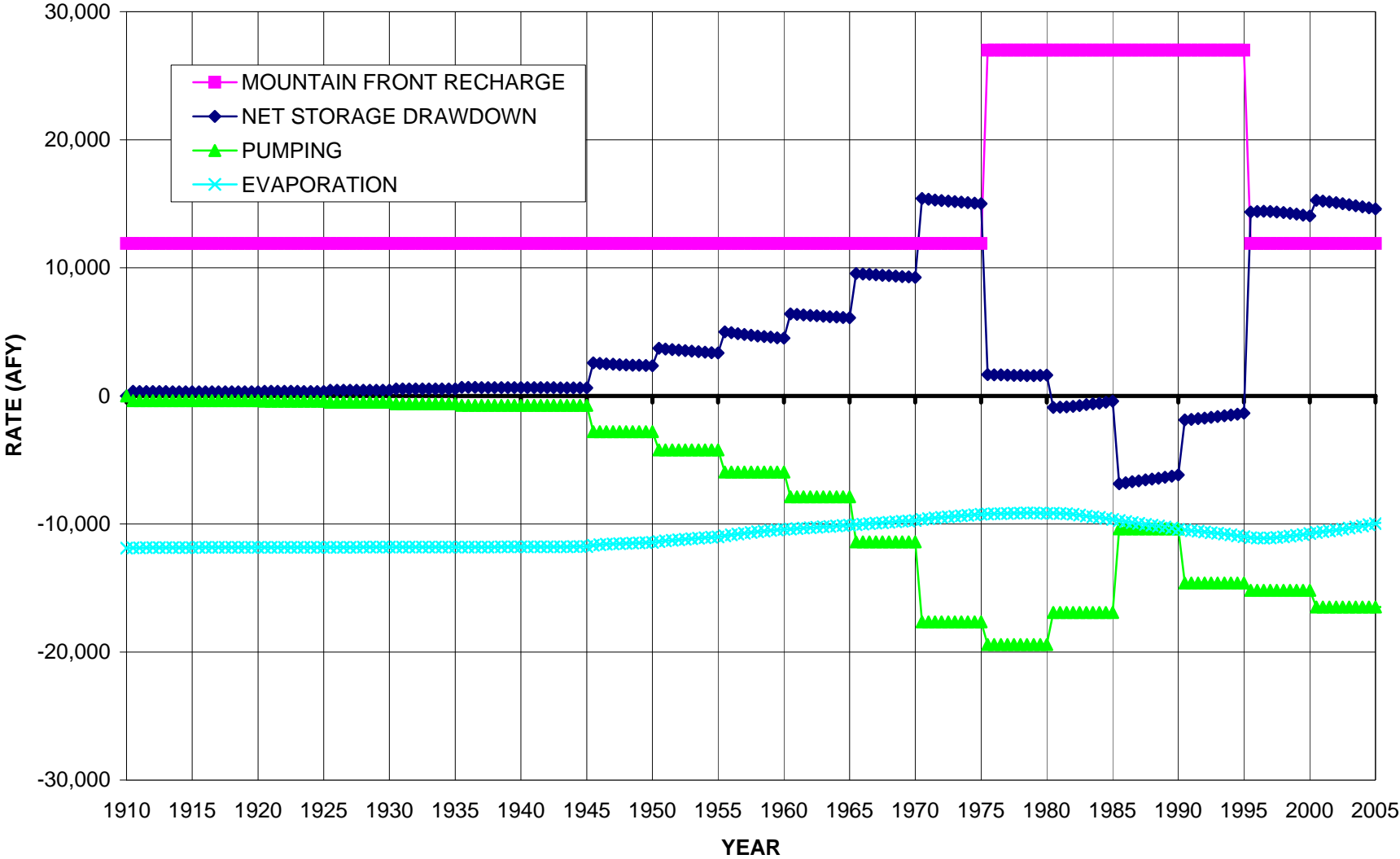


FIGURE 11
COMPARISON OF SIMULATED TO OBSERVED HYDROGRAPHS



**FIGURE 12
SIMULATED WATER BUDGET COMPONENTS**



TABLES

**TABLE 1
STEADY STATE MOUNTAIN FRONT RECHARGE**

ID#	MODEL GRID INTERSECTION		WATERSHED AREA (acres)	WATERSHED CENTROID ELEV. (ft msl)	WATERSHED CENTROID PRECIP. (in/yr)	WATERSHED RAINFALL (AFY)	WATERSHED RAINFALL PORTION	SIMULATED RECHARGE (AFY)	SIMULATED RECHARGE (CFD)
	ROW	COLUMN							
1	6	44	55,353	5749	15.3	70,755	13.11%	1,559	185,937
2	9	43	4,045	5031	12.6	4,252	0.79%	94	11,173
3	11	44	7,162	5590	14.7	8,794	1.63%	194	23,110
4	13	43	5,340	5056	12.7	5,655	1.05%	125	14,861
5	19	43	8,485	5535	14.5	10,271	1.90%	226	26,992
6	25	44	63,347	6114	16.7	88,299	16.36%	1,946	232,043
7	33	41	8,720	5082	12.8	9,307	1.72%	205	24,457
8	41	41	97,057	8039	24.0	194,464	36.04%	4,285	511,034
9	47	42	11,915	5574	14.7	14,572	2.70%	321	38,294
10	51	43	10,505	6580	18.5	16,194	3.00%	357	42,557
11	54	43	4,658	5750	15.3	5,955	1.10%	131	15,648
12	56	45	40,356	6980	20.0	67,318	12.48%	1,483	176,905
13	59	44	7,805	6367	17.7	11,505	2.13%	254	30,234
14	72	41	15,782	7010	20.1	26,478	4.91%	583	69,581
15	74	38	4,161	6095	16.7	5,775	1.07%	127	15,176
TOTAL						539,593	100.00%	11,890	1,418,001

TABLE 2
HISTORICAL SIMULATED PUMPING
ADAPTED FROM FINCH AND SHOMAKER (MARCH 2003)

ID	NMOSE	COMMENT	LOCATION (T,R,S,Q)	MODEL ROW	MODEL COLUMN	STRESS PERIOD START DATE END DATE	1	2	3	4	5	6	7	8	9	10	11	
							1/1/1910 12/31/1914	1/1/1915 12/31/1919	1/1/1920 12/31/1924	1/1/1925 12/31/1929	1/1/1930 12/31/1934	1/1/1935 12/31/1939	1/1/1940 12/31/1944	1/1/1945 12/31/1949	1/1/1950 12/31/1954	1/1/1955 12/31/1959	1/1/1960 12/31/1964	
87	T-0431		16.10.05.14	60	43	RATE	0	0	0	0	0	0	0	0	0	0	0	0
88	Alamagordo (T-0032-S-8, S-7)	shifted from (61.43)	16.10.05.42	61	42	(CFD)	0	0	0	0	0	0	0	0	0	0	2,000	2,000
89	irr-w/gw 16 acres		16.09.13.2	62	39		0	0	0	0	0	0	0	0	0	0	4,771	26,542
90	T-0065		16.10.05.33	62	41		0	0	0	0	0	0	0	0	10,000	10,000	10,000	
91	T-0176, T-0189		16.09.23.24	64	36		0	0	0	0	0	0	0	0	1,000	1,000	1,000	
92	T-1351		16.10.18.4	65	39		0	0	0	0	0	0	0	0	0	0	0	
93			16.10.18.4	65	39		0	0	0	0	0	0	0	0	0	2,000	2,000	
94			16.10.08.3	63	41		0	0	0	0	0	0	0	0	1,000	1,000	1,000	
95	T-0501		16.10.18.23	64	39		0	0	0	0	5,000	5,000	5,000	5,000	5,000	5,000	5,000	
96			16.10.17.2	64	41		0	0	0	0	0	0	0	1,000	1,000	1,000	1,000	
97	T-0779, T-0533, T-0172	subtracted from rch cell	16.09.27.21	72	41		0	0	0	0	0	0	0	0	0	0	0	
98		subtracted from rch cell	16.09.26.12	72	41		0	0	0	0	0	0	0	0	0	0	0	
99	T-1090, T-0031, T-0735, T-0639	subtracted from rch cell	16.09.25.12	72	41		0	0	0	0	0	0	14,000	7,000	7,000	10,000	10,000	
100		subtracted from rch cell	16.09.24.4	59	44		0	0	0	0	0	0	0	0	0	0	0	
101			16.10.16.2	65	43		0	0	0	1,000	1,000	1,000	1,000	2,000	2,000	2,000	2,000	
102			16.10.21.1	67	42		0	0	0	1,000	1,000	1,000	1,000	3,000	3,000	3,000	3,000	
103			16.09.34.2	67	33		0	0	0	0	0	0	0	0	0	0	0	
104	T-0051		16.09.35.22	67	36		0	0	0	0	0	0	0	20,000	15,000	15,000	15,000	
105			16.10.30.21	69	39		0	0	0	0	0	0	0	6,000	0	0	0	
106			16.10.20.4	67	41		0	0	0	0	0	0	0	0	0	0	0	
107			16.10.21.3	67	43		0	0	1,000	1,000	1,000	1,000	1,000	1,000	3,000	3,000	3,000	
108			16.10.28.1	69	41		0	0	1,000	1,000	2,000	2,000	2,000	2,000	3,000	3,000	3,000	
109			16.10.29.33	69	39		0	0	0	0	0	0	0	5,000	0	0	0	
110			16.10.32.12	70	39		0	0	0	0	0	0	0	10,000	0	0	0	
111			16.10.28.3	70	41		3,000	3,000	3,000	4,000	5,000	5,000	5,000	5,000	5,000	5,000	5,000	
112			17.09.01.3	70	35		0	0	0	0	0	0	0	0	0	0	0	
113			16.10.32.24	71	40		4,000	4,000	4,000	5,000	6,000	6,000	6,000	6,000	6,000	6,000	8,000	
114	T-1493		16.10.31.44	71	38		0	0	0	0	0	0	0	4,000	8,000	10,000	10,000	
115			16.10.32.4	71	40		5,000	5,000	5,000	8,000	10,000	10,000	10,000	10,000	10,000	10,000	12,000	
116			16.10.33.3	72	41		5,000	5,000	5,000	8,000	10,000	10,000	10,000	10,000	15,000	15,000	15,000	
117			17.10.05.4	73	40		5,000	5,000	5,000	8,000	10,000	10,000	10,000	10,000	10,000	10,000	10,000	
118			17.10.07.0	74	37		0	0	0	0	0	0	0	0	0	0	0	
119			17.10.08.1	74	39		0	0	0	0	2,000	2,000	2,000	3,000	3,000	3,000	3,000	
120	T-0111, T-0173, T-0114, T-0132-A, T-1041		17.09.24.33	76	34		0	0	0	0	0	0	0	0	0	0	0	
121	T-0821		17.09.24.31	76	34		0	0	0	0	0	0	0	0	4,431	4,702	7,323	
122	T-0115, T-1085-S-2		17.09.26.32	77	32		0	0	0	0	0	0	0	0	0	0	0	
123	T-1140, T-1085-S-3		17.09.26.22	77	33		0	0	0	0	0	0	0	0	0	500	3,000	
124			17.09.24.43	77	34		0	0	0	0	0	0	0	0	2,773	14,106	21,968	
125			17.09.24.44	77	35		0	0	0	0	0	0	0	8,521	27,192	23,511	36,613	
126			17.10.18.44	77	37		0	0	0	0	0	0	0	0	2,773	4,702	7,323	
127			17.09.25.2	77	35		0	0	0	0	0	0	0	0	0	0	0	
128			17.10.19.3	78	35		0	0	0	0	0	0	0	3,535	6,663	4,702	7,323	
129	T-2333		17.10.30.31	80	35		0	0	0	0	0	0	0	15,000	15,500	15,500	10,000	
130	T-0032, T-0507		17.09.35.24	79	32		0	0	0	0	0	0	0	2,710	4,379	4,379	4,379	
131	T-0032-S		17.09.35.44	80	32		0	0	0	0	0	0	0	2,710	4,379	4,379	4,379	
132	HAFB (T-0756-S)		17.10.32.11	81	36		0	0	0	0	0	0	0	0	0	0	11,732	
133	HAFB (T-1255-S, S-3, S-4, S-5, T-0756-S-4)		17.10.31.40	83	35		0	0	0	0	0	0	0	0	0	0	15,560	
134	T-0079		18.09.11.32	83	30		0	0	0	0	0	0	0	0	0	0	3,000	
135	HAFB (T-1255-S-2)		17.10.31.44	83	35		0	0	0	0	0	0	0	0	0	0	11,930	
136			18.10.06.2	83	35		0	0	0	0	0	0	0	0	0	0	9,209	
137	T-1058		18.09.13.22	85	33		0	0	0	0	0	0	0	0	0	0	0	
SUM (CFD)							48,000	48,000	53,000	64,000	77,000	92,000	92,000	336,856	507,262	714,470	943,471	
SUM (AFY)							402	402	444	537	646	771	771	2,825	4,253	5,991	7,911	

TABLE 2
HISTORICAL SIMULATED PUMPING
ADAPTED FROM FINCH AND SHOMAKER (MARCH 2003)

ID	NMOSE	COMMENT	LOCATION (T.R.S.QOO)	MODEL ROW	MODEL COLUMN	STRESS PERIOD START DATE END DATE	12	13	14	15	16	17	18	19
							1/1/1965	1/1/1970	1/1/1975	1/1/1980	1/1/1985	1/1/1990	1/1/1995	1/1/2000
1	Three Rivers Cattle T-442 et al (T-442)		11.09.34.4	8	42		20,500	3,908	3,908	3,908	3,908	3,908	3,908	3,908
2	Three Rivers Cattle T-442 et al (T-442(2))	subtracted from rch cell		6	44		20,500	3,908	3,908	3,908	3,908	3,908	3,908	3,908
3	Three Rivers Cattle T-442 et al	shifted from (7.45)		6	45		9,000	0	7,616	7,816	7,816	7,816	7,816	7,816
4	Three Rivers Cattle T-442 et al			8	41		10,010	0	0	7,816	11,781	15,631	23,447	
5	Niccum (T-2014, T-2016, T-2018, T-2023, T-2024)		12.09.10.22	10	41		10,010	55,814	0	0	0	0	0	0
6	Niccum (T-2019)		12.09.11.11	10	42		3,000	11,163	0	0	0	0	0	0
7	Niccum (T-2017, T-2020, T-2022, T-2026)		12.09.11.33	12	41		10,200	44,651	0	0	0	0	0	0
8	Niccum (T-2021)		12.09.14.22	13	43		25,000	11,163	0	0	0	0	0	0
9	HFR T-1797-S-8			29	40		50,000	0	0	0	21,271	32,975	42,908	
10	HFR T-1797-S-6&7		13.09.23.4	28	38		15,000	0	0	0	21,271	32,975	42,908	
11	HFR T-1797-S-5		13.09.24.2	27	41		0	45,000	20,500	20,500	21,271	32,975	42,908	
12	HFR T-1797-S-4			29	40		20,500	23,000	23,676	48,510	29,815	21,271	32,975	42,908
13	HFR T-1797-S-3		13.09.25.0	29	40		9,000	25,000	28,298	9,048	29,815	21,271	32,975	42,908
14	HFR T-1797-S-			31	39		5,005	24,000	25,988	15,997	14,919	21,271	32,975	42,908
15	T-0028 HFR (T-1797)		13.09.36.23	31	39		5,005	30,000	25,988	15,997	14,919	21,271	32,975	42,908
16	T-594, T-774		14.09.10.31	34	33		5,100	30,000	3,000	3,000	0	3,000	3,000	3,000
17	irr-w/gw 160 acres (same OSE cell as Hydrograph		14.09.01.3	34	38		10,200	3,000	10,200	10,200	10,200	11,503	11,503	12,906
18	irr-w/gw 70 acres		14.09.16.0	36	32		15,000	25,600	25,000	15,000	5,100	5,752	6,403	
19	T-768		14.09.11.44	36	37		0	10,000	50,000	50,000	0	5,000	5,000	0
20	irr-w/gw 355 acres (same OSE cell as Hyd. 7) T-0		14.09.15.3	36	33		15,000	10,000	15,000	15,000	10,000	11,277	11,277	12,555
21	T-0085, T-0070 (Hydrograph 8)		14.09.22.22	37	34		25,000	25,000	50,000	61,400	61,400	69,244	69,244	77,087
22	T-0929		14.09.13.32	37	37		23,000	30,000	9,000	13,400	13,400	15,112	15,112	16,824
23	T-156, T-157		14.10.18.0	34	28		15,400	3,000	25,600	33,900	25,000	38,231	38,231	42,561
24	T-0055, T-0021		14.09.23.23	38	35		18,000	20,000	24,000	20,000	11,500	12,969	12,969	14,438
25	T-0085-S (see Hyd. 9), T-0723		14.09.24.12	38	37		28,200	51,000	28,200	20,000	20,000	12,969	12,969	14,438
26	T-0022		14.10.17.41	35	30		20,000	30,000	30,000	30,000	11,500	12,969	12,969	14,438
27	T-0188		14.10.20.44	38	30		3,000	3,000	3,000	3,000	3,000	3,000	3,000	3,000
28	T-0730		14.09.27.23	40	33		25,600	13,000	25,000	10,000	4,500	5,075	5,075	5,650
29	T-14		14.10.19.31	36	26		5,000	40,000	20,000	20,000	0	10,000	10,000	0
30	T-104		14.09.25.22	40	37		2,500	15,000	20,000	20,000	0	10,000	10,000	0
31	T-0018		14.10.19.14	36	27		25,000	10,000	25,000	15,000	9,100	10,262	10,262	11,425
32	T-25		14.10.19.23	36	27		20,000	18,000	30,000	30,000	0	10,000	10,000	0
33	T-0443, T-0057 (Hydrograph 17)		14.10.20.22	36	30		3,000	5,000	3,000	3,000	3,000	3,000	3,000	3,000
34	T-0057-A, T-589		14.10.20.14	37	29		18,000	12,000	20,000	15,000	8,600	9,699	9,699	10,797
35	T-0027, T-0158, T-0001, T-0004, T-0170, T-0169		14.09.26.41	41	35		48,600	30,000	55,000	49,000	30,000	55,260	55,260	61,519
36	T-61		14.09.26.42	41	35		20,000	2,000	40,000	40,000	0	10,000	10,000	10,000
37	T-0077		14.10.20.42	37	36		3,000	8,000	4,800	6,500	6,500	6,947	6,947	7,394
38	T-1494		14.09.35.11	42	33		10,200	28,700	13,000	10,000	7,700	8,684	8,684	9,667
39	T-0046 (Hydrograph 10)		14.09.25.32	41	36		40,000	35,000	64,000	31,700	31,700	35,750	35,750	39,799
40	T-0484, T-0013		14.10.30.32	42	38		13,400	10,000	33,000	33,000	33,000	37,216	37,216	41,431
41			14.09.36.12	42	36		1,000	10,000	20,000	20,000	0	10,000	10,000	10,000
42	T-0010, T-0076 (Hydrograph 18)		14.10.29.31	42	40		10,000	5,000	20,500	23,000	10,000	25,938	25,938	28,676
43	T-216, T-1363, T-1359 (in)		14.10.29.14	43	40		1,000	25,000	10,000	10,000	5,000	5,000	5,000	5,000
44	T-216, T-1363, T-1359 (in)		14.09.35.4	43	34		12,000	10,000	12,000	8,300	8,300	9,360	9,360	10,421
45	T-467		14.09.36.24	43	37		20,000	15,000	41,000	21,800	21,800	24,585	24,585	27,370
46	irr-w/gw 35 acres		14.10.32.1	43	39		2,000	10,000	2,000	1,900	1,900	2,143	2,143	2,385
47	T-0879		15.09.02.24	44	34		2,600	1,000	12,000	7,680	7,680	8,661	8,661	9,642
48	T-0835 (Hydrograph 21)		15.09.01.12	44	35		25,000	5,000	32,400	46,078	46,078	51,964	51,964	57,850
49	T-0019, T-1319		15.10.06.11	45	37		35,000	8,000	35,000	7,700	7,700	8,684	8,684	9,667
50	T-0223, T-0686, T-0218, T-1003, T-428, T-960		15.10.08.42	46	38		10,000	10,000	20,000	8,960	8,960	10,105	10,105	11,249
51			15.10.05.3	46	38		5,000	10,000	20,000	20,000	6,800	7,669	7,669	8,537
52	T-0164, T-1057		15.10.04.13	46	40		5,000	20,000	10,000	10,000	0	5,000	5,000	5,000
53			15.09.12.41	47	35		20,500	5,000	38,000	30,000	4,480	5,052	5,052	5,625
54	T-0178-S, T-0178		15.10.07.31	47	36		10,000	0	5,000	2,560	2,560	2,887	2,887	3,214
55			15.10.07.24	47	38		10,000	0	30,000	30,000	0	10,000	10,000	0
56	T-0948		15.10.09.14	48	46		10,000	20,000	10,000	10,000	2,000	2,255	2,255	2,511
57	T-107		15.10.08.41	48	39		1,000	10,000	1,000	1,300	1,300	1,466	1,466	1,632
58			15.09.13.42	49	35		5,000	2,600	5,000	5,000	0	5,000	0	0
59	T-0155, T-1628		15.10.09.40	49	41		7,000	20,000	8,000	7,680	7,860	8,661	8,661	9,642
60	T-1247		15.10.10.13	49	42		0	10,000	10,000	10,000	1,640	1,850	1,850	2,059
61	T-0190		15.10.18.33	50	35		10,000	2,000	10,000	10,000	0	5,000	0	0
62	irr-w/gw 32 acres; T-1068		15.10.17.3	50	37		20,000	3,800	20,000	6,400	6,400	7,218	7,218	8,035
63	T-0406, T-0405, T-1274, T-1306, T-1307, T-0980		15.10.16.14	50	40		0	2,000	5,000	5,760	5,760	6,496	6,496	7,232
64	T-0802		15.10.19.31	52	35		0	12,000	0	1,300	1,300	1,466	1,466	1,632
65	T-1204		15.10.21.14	52	39		0	2,000	2,300	2,300	0	0	0	0
66			15.10.21.42	53	40		2,000	0	30,000	30,000	0	10,000	10,000	10,000
67			15.10.29.13	53	38		2,000	40,000	20,000	20,000	0	10,000	10,000	10,000
68	irr-w/gw 32 acres see #43 (Hydrograph 27)		15.10.29.1	53	37		2,600	4,800	2,600	2,600	0	0	0	0
69	T-1626		15.10.22.32	53	41		20,000	0	20,000	8,320	8,320	9,383	9,383	10,446
70			15.10.21.44	53	40		5,000	0	20,000	20,000	0	10,000	0	0
71	irr-w/gw 24 acres		15.10.24.11	53	45		2,000	52,749	2,000	2,000	2,000	2,000	2,000	2,000
72	T-1151, T-0572, T-0195, T-1312		15.10.28.13	54	38		0	3,000	3,800	3,800	4,331	4,331	4,331	4,821
73	irr-w/gw 36 acres		15.10.24	54	45		2,000	3,000	2,000	2,000	2,000	2,000	2,000	2,000
74	irr-w/gw 3 acres		15.10.26	55	45		10,000	10,000	12,000	12,000	0	10,000	10,000	10,000
75	irr-w/gw 1 acre		15.10.25.1	55	44		2,							

TABLE 2
HISTORICAL SIMULATED PUMPING
ADAPTED FROM FINCH AND SHOMAKER (MARCH 2003)

ID	NMOSE	COMMENT	LOCATION (T&S COORD)	MODEL ROW	MODEL COLUMN	STRESS PERIOD									
						12 1/1/1965 12/31/1969	13 1/1/1970 12/31/1974	14 1/1/1975 12/31/1979	15 1/1/1980 12/31/1984	16 1/1/1985 12/31/1989	17 1/1/1990 12/31/1994	18 1/1/1995 12/31/1999	19 1/1/2000 6/30/2005		
87	T-0431		16.10.05.14	60	42	3,100	0	3,100	3,072	6,272	7,073	7,073	7,073	7,875	
88	Alamagordo (T-0032-S-8, S-7)	shifted from (61,43)	16.10.05.42	61	42	53,871	32,000	88,743	95,476	43,410	57,436	120,465	120,465	166,965	
89	irr-w/gw 16 acres		16.09.13.2	62	39	13,000	10,200	20,000	11,520	11,520	12,992	12,992	14,463		
90	T-0065		16.10.05.33	62	41	1,000	0	1,000	1,000	1,000	1,000	1,000	1,000		
91	T-0176, T-0189		16.09.23.24	64	36	500	2,000	20,000	20,000	3,840	4,331	4,331	4,821		
92	T-1351		16.10.18.4	65	39	3,100	3,000	3,100	3,072	5,972	6,734	6,734	7,498		
93			16.10.18.4	65	39	2,600	1,500	2,600	2,560	5,160	5,819	5,819	6,478		
94			16.10.08.3	63	41	1,000	30,000	1,000	1,000	1,000	1,000	1,000	1,000		
95	T-0501		16.10.18.23	64	39	6,400	10,000	6,400	6,400	12,800	14,436	14,436	16,070		
96			16.10.17.2	64	41	1,000	0	1,000	1,000	1,000	1,000	1,000	1,000		
97	T-0779, T-0533, T-0172	subtracted from rch cell	16.09.27.21	72	41	0	2,000	0	1,024	1,024	1,155	1,155	1,286		
98		subtracted from rch cell	16.09.26.12	72	41	32,000	2,000	40,000	30,000	17,279	19,486	19,486	21,694		
99	T-1090, T-0031, T-0735, T-0639	subtracted from rch cell	16.09.25.12	72	41	10,200	5,000	20,000	20,000	11,519	11,770	11,770	11,770		
100		subtracted from rch cell	16.09.24.4	58	44	0	10,000	0	5,800	5,800	6,541	7,282	7,282		
101			16.10.16.2	65	43	2,000	4,000	2,000	2,000	2,000	2,000	2,000	2,000		
102			16.10.21.1	67	42	3,000	0	3,000	5,000	5,000	5,000	5,000	5,000		
103			16.09.34.2	67	33	1,500	8,000	1,500	1,279	1,279	1,442	1,442	1,606		
104	T-0051		16.09.35.22	67	36	30,700	10,000	40,000	30,000	19,839	22,373	22,373	24,908		
105			16.10.30.21	68	39	5,000	12,000	20,000	20,000	0	10,000	10,000	10,000		
106			16.10.20.4	67	41	0	20,000	0	3,800	7,640	8,616	8,616	9,892		
107			16.10.21.3	67	43	3,000	10,000	3,000	5,000	5,000	5,000	5,000	5,000		
108			16.10.28.1	69	41	3,000	5,000	3,000	6,000	6,000	6,000	6,000	6,000		
109			16.10.29.33	69	39	5,000	3,000	5,000	10,000	0	10,000	10,000	10,000		
110			16.10.32.12	70	39	5,000	17,000	20,000	20,000	0	10,000	10,000	10,000		
111			16.10.28.3	70	41	5,000	7,693	5,000	8,000	8,000	8,000	8,000	8,000		
112			17.09.01.3	70	35	0	5,000	0	1,300	1,300	1,466	1,466	1,632		
113			16.10.32.24	71	40	8,000	7,000	8,000	1,000	10,000	10,000	10,000	10,000		
114	T-1493		16.10.31.44	71	38	10,000	17,371	28,295	28,295	28,295	31,910	31,910	35,524		
115			16.10.32.4	71	40	12,000	13,840	12,000	12,000	15,512	15,577	15,577	15,643		
116			16.10.33.3	72	41	20,000	8,031	20,000	25,000	25,000	25,000	25,000	25,000		
117			17.10.05.4	73	40	10,000	0	10,000	15,000	15,000	15,000	15,000	15,000		
118			17.10.07.0	74	37	0	2,463	5,100	12,000	12,000	13,533	13,533	15,066		
119			17.10.08.1	74	39	3,000	20,000	3,000	4,000	4,000	4,000	4,000	4,000		
120	T-0111, T-0173, T-0114, T-0132-A, T-1041		17.09.24.33	76	34	15,000	4,379	17,000	16,639	16,639	18,765	18,765	20,890		
121	T-0821		17.09.24.31	76	34	7,028	4,379	7,794	7,681	7,681	8,662	8,662	9,643		
122	T-0115, T-1085-S-2		17.09.26.32	77	32	2,600	34,167	2,600	7,680	7,680	8,661	8,661	9,642		
123	T-1140, T-1085-S-3		17.09.26.22	77	33	5,000	67,286	7,600	17,600	17,600	19,848	19,848	22,097		
124			17.09.24.43	77	34	17,371	7,000	17,837	24,092	24,092	27,170	27,170	30,247		
125			17.09.24.44	77	35	18,236	155,813	12,745	15,957	15,957	17,995	17,995	20,034		
126			17.10.18.44	77	37	11,833	7,693	11,732	14,861	14,861	16,759	16,759	18,658		
127			17.09.25.2	77	35	0	20,000	0	600	600	677	677	753		
128			17.10.19.3	78	35	3,302	2,463	1,322	2,069	2,069	2,333	2,333	2,598		
129	T-2333		17.10.30.31	80	35	10,000	20,000	40,000	40,000	0	10,000	10,000	0		
130	T-0032, T-0507		17.09.35.24	79	32	4,379	4,379	4,379	4,379	0	0	0	0		
131	T-0032-S		17.09.35.44	80	32	4,379	4,379	4,379	4,379	0	0	0	0		
132	HAFB (T-0756-S)		17.10.32.11	81	36	41,578	34,167	16,558	13,847	13,847	19,568	14,025	14,192		
133	HAFB (T-1255-S, S-3, S-4, S-5, T-0756-S-4)		17.10.31.40	83	35	43,693	67,286	49,623	41,004	41,004	64,296	46,082	46,631		
134	T-0079		18.09.11.32	83	30	3,000	7,000	7,000	2,560	2,560	2,887	2,887	3,214		
135	HAFB (T-1255-S-2)		17.10.31.44	83	35	58,913	155,813	139,330	124,621	115,573	195,683	140,251	141,920		
136			18.10.06.2	83	35	10,176	7,693	23,006	23,006	0	15,000	15,000	0		
137	T-1058		18.09.13.22	85	33	20,000	20,000	40,000	40,000	0	10,000	0	0		
SUM (CFD)						1,363,565	2,181,738	2,323,660	2,024,997	1,245,787	1,752,296	1,818,926	1,974,607		
SUM (AFY)						11,434	18,294	19,484	16,980	10,446	14,693	15,252	16,557		

**TABLE 3
TULAROSA BASIN AQUIFER TEST INFORMATION**

id #	Location (T.R.S.QQQ)	Test Transmissivity (ft²/day)	Calibrated Transmissivity (ft²/day)	Source
1	11S.9E.34	6000	5000	Morrison (1989)
2	13S.9E.1.341	5880	3000	JSAI T-3825 pump test (2003)
3	14S.10E.18.424	400	900	Morrison (1989)
4	14S.9E.11.422	2150	900	Morrison (1989)
5	14S.9E.36.422	5000	4000	Morrison (1989)
6	15S.10E.36.111	2655	3000	JSAI (2003)
7	16S.10E.5.244	2600	3000	JSAI (2003)
8	16S.10E.5.444	6244	off grid	JSAI (2003)
9	16S.8E.13.400	60	900	Morrison (1989)
10	16S.9E.4.400	380	3000	Morrison (1989)
11	16S.9E.8.100	160	900	Morrison (1989)
12	17S.10E.18.432	180	900	Morrison (1989)
13	17S.10E.18.442	600	900	Morrison (1989)
14	17S.10E.19.112	1330	900	Morrison (1989)
15	17S.10E.19.112	1370	900	Morrison (1989)
16	17S.10E.19.112	1590	900	Morrison (1989)
17	17S.10E.19.112	14400	900	Morrison (1989)
18	17S.10E.19.113	200	900	Morrison (1989)
19	17S.10E.19.121	600	900	Morrison (1989)
20	17S.10E.19.122	1600	900	Morrison (1989)
21	17S.10E.19.123	2130	900	Morrison (1989)
22	17S.10E.19.123	8528	900	Morrison (1989)
23	17S.10E.19.123	8020	900	Morrison (1989)
24	17S.10E.19.141	720	900	Morrison (1989)
25	17S.10E.19.142	1870	900	Morrison (1989)
26	17S.10E.19.142	1730	900	Morrison (1989)
27	17S.10E.19.144	2340	900	Morrison (1989)
28	17S.10E.19.321	1400	900	Morrison (1989)
29	17S.10E.31.424	1160	900	Morrison (1989)
30	17S.10E.32.234	20000	900	Morrison (1989)
31	17S.9E.24.342	2700	900	Morrison (1989)
32	17S.9E.25.212	1560	900	Morrison (1989)
33	17S.9E.25.213	2000	900	Morrison (1989)
34	17S.9E.25.222	2000	900	Morrison (1989)
35	16S.9E.36	600	600	USBR (2003)
36	13S.9E.36.214	214	900	JSAI T-71 specific capacity
37	13S.9E.36.442	2874	900	JSAI T-564-s specific capacity
38	12S.9E.3.444	227	5000	JSAI T-2014 specific capacity
39	12S.9E.10.244	856	5000	JSAI T-2016 specific capacity
40	12S.9E.14.331	321	300	JSAI T-2017 specific capacity
41	12S.9E.3.422	3369	5000	JSAI T-2018 specific capacity
42	12S.9E.11.144	842	5000	JSAI T-2019 specific capacity
43	12S.9E.11.344	1303	5000	JSAI T-2020 specific capacity
44	12S.9E.14.241	515	300	JSAI T-2021 specific capacity
45	12S.9E.14.324	856	300	JSAI T-2022 specific capacity
46	12S.9E.10.233	1578	5000	JSAI T-2023 specific capacity
47	12S.9E.11.331	1872	5000	JSAI T-2026 specific capacity
48	13S.9E.1.341	2767	3000	JSAI T-3825 specific capacity
49	13S.9E.36.424	2219	900	JSAI T-1797 specific capacity
50	13S.9E.36	5147	900	JSAI T-1797-s specific capacity
51	13S.9E.25	1471	3000	JSAI T-1797-s-3 specific capacity
52	13S.9E.25	8890	900	JSAI T-1797-s-4 specific capacity

**TABLE 4
OBSERVED AND COMPUTED STEADY STATE WATER ELEVATIONS**

ID#	T.R.S	UTM X	UTM Y	Observed (ft msl)	Computed (ft msl)	Residual (ft)
1	T11S.R09E.27	400,863	3,689,118	4557	4534	23
2	T11S.R09E.22	400,879	3,690,658	4630	4507	123
3	T11S.R09E.19	395,241	3,690,347	4361	4328	33
4	T11S.R09E.19	395,267	3,690,409	4387	4329	58
5	T12S.R09E.3	399,851	3,686,202	4280	4318	-38
6	T12S.R09E.3	400,834	3,686,223	4270	4320	-50
7	T12S.R09E.3	400,231	3,685,427	4266	4315	-49
8	T12S.R09E.11	402,236	3,684,144	4352	4340	12
9	T12S.R09E.11	401,430	3,683,752	4327	4315	12
10	T12S.R09E.10	401,024	3,684,588	4284	4314	-30
11	T12S.R09E.10	401,016	3,683,787	4315	4313	2
12	T12S.R09E.14	401,827	3,682,116	4314	4331	-17
13	T12S.R09E.14	402,604	3,682,139	4324	4346	-22
14	T12S.R09E.19	394,697	3,680,804	4253	4269	-16
15	T13S.R10E.6	404,551	3,674,943	4388	4396	-8
16	T13S.R09E.20	397,517	3,670,886	4301	4278	23
17	T13S.R09E.36	403,417	3,667,654	4378	4359	19
18	T13S.R09E.34	400,380	3,667,100	4356	4326	30
19	T14S.R09E.4	398,014	3,666,293	4241	4261	-20
20	T14S.R09E.1	403,871	3,666,387	4403	4358	45
21	T14S.R09E.12	403,646	3,664,634	4384	4349	35
22	T14S.R09E.13	403,683	3,663,001	4340	4344	-4
23	T14S.R10E.18	405,647	3,662,365	4365	4389	-24
24	T14S.R09E.22	399,835	3,661,900	4289	4289	0
25	T14S.R09E.22	399,705	3,661,932	4304	4286	18
26	T14S.R10E.20	405,794	3,661,502	4359	4401	-42
27	T14S.R10E.18	405,642	3,661,934	4384	4393	-9
28	T14S.R10E.17	405,903	3,662,056	4374	4398	-24
29	T14S.R09E.23	401,182	3,661,825	4307	4310	-3
30	T14S.R09E.22	400,111	3,661,065	4228	4292	-64
31	T14S.R10E.19	405,686	3,661,133	4434	4399	35
32	T14S.R10E.19	404,881	3,660,987	4370	4376	-6
33	T14S.R10E.19	405,143	3,661,232	4374	4383	-9
34	T14S.R09E.21	398,030	3,660,409	4267	4255	12
35	T14S.R09E.24	402,957	3,660,390	4291	4334	-43
36	T14S.R10E.30	404,949	3,659,939	4368	4375	-7
37	T14S.R09E.26	401,264	3,659,730	4291	4309	-18
38	T14S.R09E.27	400,483	3,659,398	4265	4298	-33
39	T14S.R09E.25	403,154	3,659,341	4274	4336	-62
40	T14S.R09E.25	403,258	3,659,402	4274	4338	-64
41	T14S.R10E.29	405,955	3,659,436	4371	4393	-22
42	T14S.R09E.26	402,451	3,659,101	4280	4324	-44
43	T14S.R09E.26	402,065	3,659,382	4288	4320	-32
44	T14S.R10E.32	406,594	3,658,476	4380	4385	-5
45	T14S.R10E.32	406,413	3,658,508	4383	4383	0
46	T14S.R09E.36	403,146	3,658,571	4312	4333	-21
47	T14S.R09E.36	403,561	3,658,598	4315	4339	-24

**TABLE 4
OBSERVED AND COMPUTED STEADY STATE WATER ELEVATIONS**

ID#	T.R.S	UTM X	UTM Y	Observed (ft msl)	Computed (ft msl)	Residual (ft)
48	T14S.R09E.25	403,254	3,658,970	4279	4336	-57
49	T14S.R09E.36	402,782	3,658,483	4307	4327	-20
50	T14S.R10E.31	404,800	3,657,938	4366	4354	12
51	T14S.R10E.31	404,542	3,658,126	4370	4352	18
52	T14S.R09E.34	400,727	3,657,795	4271	4299	-28
53	T14S.R09E.34	400,731	3,658,195	4280	4300	-20
54	T14S.R09E.35	402,357	3,657,439	4285	4317	-32
55	T14S.R10E.31	405,364	3,657,287	4362	4357	5
56	T14S.R09E.35	401,656	3,657,385	4257	4308	-51
57	T14S.R09E.35	401,550	3,657,109	4278	4305	-27
58	T15S.R09E.1	403,129	3,656,877	4331	4324	7
59	T15S.R10E.6	404,419	3,656,064	4325	4335	-10
60	T15S.R09E.2	401,413	3,656,402	4267	4299	-32
61	T15S.R10E.6	404,109	3,656,221	4350	4333	17
62	T15S.R09E.1	403,126	3,656,539	4319	4322	-3
63	T15S.R10E.7	404,281	3,655,234	4343	4324	19
64	T15S.R10E.7	405,526	3,655,222	4365	4338	27
65	T15S.R10E.7	405,129	3,654,425	4347	4324	23
66	T15S.R10E.7	404,709	3,653,998	4336	4314	22
67	T15S.R09E.13	403,871	3,653,143	4308	4294	14
68	T15S.R09E.24	403,935	3,651,665	4236	4279	-43
69	T15S.R09E.24	403,961	3,651,725	4232	4280	-48
70	T15S.R10E.22	410,004	3,651,237	4356	4334	22
71	T15S.R09E.24	403,930	3,651,140	4243	4275	-32
72	T15S.R10E.22	409,947	3,650,776	4342	4331	11
73	T15S.R10E.29	406,723	3,650,067	4272	4294	-22
74	T15S.R10E.29	406,622	3,650,407	4324	4297	28
75	T15S.R10E.30	405,478	3,650,294	4262	4284	-22
76	T15S.R09E.29	396,100	3,649,496	4137	4138	-1
77	T15S.R10E.30	404,740	3,649,039	4240	4268	-28
78	T15S.R10E.36	412,239	3,648,753	4342	4349	-7
79	T16S.R09E.6	401,373	3,647,316	4206	4206	0
80	T16S.R08E.1	400,276	3,646,649	4160	4178	-18
81	T16S.R08E.1	400,277	3,646,680	4140	4178	-38
82	T16S.R09E.5	403,444	3,646,680	4209	4242	-33
83	T16S.R08E.5	392,378	3,646,270	4074	4063	11
84	T16S.R08E.6	390,820	3,646,318	4050	4037	13
85	T16S.R10E.6	410,089	3,646,309	4330	4296	35
86	T16S.R09E.3	406,479	3,646,342	4280	4267	13
87	T16S.R09E.3	406,636	3,646,433	4276	4269	8
88	T16S.R09E.9	403,824	3,645,659	4233	4240	-7
89	T16S.R08E.12	399,712	3,644,807	4148	4144	4
90	T16S.R09E.7	401,609	3,644,942	4193	4185	8
91	T16S.R08E.12	399,449	3,644,502	4139	4135	4
92	T16S.R09E.9	405,007	3,644,416	4230	4243	-13
93	T16S.R08E.17	392,686	3,643,557	4056	4058	-2
94	T16S.R09E.13	408,916	3,643,178	4279	4260	19

**TABLE 4
OBSERVED AND COMPUTED STEADY STATE WATER ELEVATIONS**

ID#	T.R.S	UTM X	UTM Y	Observed (ft msl)	Computed (ft msl)	Residual (ft)
95	T16S.R09E.13	409,021	3,643,269	4276	4261	15
96	T16S.R08E.14	397,846	3,642,701	4074	4085	-11
97	T16S.R08E.14	398,686	3,643,555	4093	4106	-13
98	T16S.R09E.17	403,197	3,642,678	4200	4194	6
99	T16S.R08E.13	400,265	3,642,985	4139	4132	7
100	T16S.R08E.24	399,090	3,642,472	4124	4104	20
101	T16S.R08E.29	392,710	3,640,939	4025	4038	-13
102	T16S.R09E.26	407,956	3,640,476	4245	4235	10
103	T16S.R08E.29	392,491	3,639,955	4031	4030	1
104	T16S.R08E.29	392,311	3,640,172	4021	4031	-10
105	T16S.R09E.26	407,247	3,639,683	4234	4220	15
106	T16S.R10E.30	410,900	3,638,448	4265	4237	28
107	T16S.R08E.31	392,183	3,637,926	4006	4021	-15
108	T17S.R09E.2	406,839	3,637,654	4206	4175	31
109	T17S.R09E.1	408,811	3,637,296	4194	4194	0
110	T17S.R09E.3	405,226	3,637,576	4142	4151	-9
111	T17S.R09E.5	402,602	3,637,664	4114	4118	-4
112	T17S.R09E.5	402,576	3,637,664	4107	4118	-11
113	T17S.R09E.2	407,976	3,637,027	4176	4179	-3
114	T17S.R09E.2	408,162	3,637,488	4174	4189	-15
115	T16S.R10E.31	410,815	3,637,678	4260	4229	31
116	T17S.R09E.1	408,390	3,636,838	4141	4181	-40
117	T17S.R10E.6	410,619	3,636,140	4181	4205	-24
118	T17S.R09E.4	404,097	3,636,355	4132	4119	13
119	T17S.R09E.2	406,722	3,636,269	4150	4149	1
120	T17S.R09E.1	409,035	3,636,278	4187	4181	6
121	T17S.R09E.11	408,174	3,635,916	4177	4163	15
122	T17S.R10E.6	410,305	3,635,835	4192	4193	-1
123	T17S.R10E.6	410,383	3,635,927	4202	4197	6
124	T17S.R09E.8	403,331	3,635,193	4109	4096	13
125	T17S.R09E.8	403,333	3,635,377	4082	4098	-16
126	T17S.R09E.12	409,465	3,635,011	4192	4163	29
127	WHITE SANDS	381,382	3,632,413	3986	3959	28
128	T17S.R09E.12	409,853	3,634,730	4165	4163	2
129	T17S.R08E.13	399,447	3,634,092	4065	4049	16
130	T17S.R08E.13	398,537	3,634,132	4053	4042	11
131	T17S.R08E.13	398,616	3,634,192	4050	4044	7
132	T17S.R09E.13	409,919	3,633,406	4145	4132	13
133	T17S.R09E.13	409,817	3,633,715	4133	4139	-6
134	T17S.R09E.15	406,413	3,633,869	4100	4107	-7
135	WHITE SANDS	382,202	3,631,356	3987	3961	26
136	T17S.R09E.24	409,913	3,632,759	4116	4117	-1
137	T17S.R09E.23	408,193	3,632,313	4073	4096	-23
138	WHITE SANDS	388,193	3,632,118	3964	3973	-9
139	T17S.R09E.24	409,070	3,631,596	4084	4090	-6
140	T17S.R09E.24	408,997	3,632,182	4100	4099	1
141	T17S.R10E.18	411,097	3,631,455	4080	4094	-14

**TABLE 4
OBSERVED AND COMPUTED STEADY STATE WATER ELEVATIONS**

ID#	T.R.S	UTM X	UTM Y	Observed (ft msl)	Computed (ft msl)	Residual (ft)
142	T17S.R10E.18	410,994	3,631,518	4132	4095	37
143	T17S.R10E.18	411,074	3,631,732	4083	4100	-17
144	T17S.R10E.19	410,706	3,631,335	4096	4092	4
145	T17S.R10E.19	410,290	3,631,339	4088	4091	-3
146	T17S.R10E.19	410,368	3,631,399	4086	4092	-6
147	T17S.R09E.25	409,507	3,631,038	4066	4083	-17
148	T17S.R09E.25	409,846	3,631,158	4083	4087	-4
149	T17S.R10E.19	410,029	3,631,218	4079	4088	-9
150	T17S.R09E.25	408,750	3,630,768	4061	4076	-15
151	T17S.R09E.25	409,220	3,630,917	4057	4081	-24
152	T17S.R09E.25	408,675	3,631,108	4071	4081	-10
153	T17S.R09E.24	408,755	3,631,230	4078	4083	-5
154	T17S.R10E.19	411,507	3,630,743	4133	4081	52
155	T17S.R10E.19	411,119	3,630,992	4080	4086	-6
156	T17S.R09E.26	407,997	3,630,898	4039	4074	-35
157	T17S.R10E.19	410,413	3,630,537	4059	4078	-19
158	T17S.R10E.19	411,038	3,630,655	4076	4080	-4
159	T17S.R10E.19	410,858	3,630,871	4079	4084	-5
160	T17S.R10E.19	410,312	3,630,969	4078	4085	-7
161	T17S.R10E.19	411,067	3,631,055	4078	4087	-9
162	T17S.R10E.19	410,462	3,630,229	4060	4074	-14
163	T17S.R10E.19	410,022	3,630,479	4060	4077	-17
164	T17S.R10E.19	410,023	3,630,602	4038	4079	-41
165	T17S.R10E.19	409,997	3,630,633	4060	4079	-19
166	T17S.R10E.19	410,285	3,630,722	4089	4081	8
167	T17S.R09E.25	408,588	3,630,092	4043	4067	-24
168	T17S.R09E.26	407,546	3,629,886	4044	4060	-16
169	T17S.R10E.30	410,039	3,629,462	4063	4063	0
170	T17S.R09E.36	409,856	3,629,464	4056	4063	-7
171	T17S.R09E.26	407,025	3,629,921	4066	4058	8
172	T17S.R09E.25	409,286	3,629,685	4051	4065	-14
173	T17S.R09E.36	408,815	3,629,381	4050	4059	-9
174	T17S.R09E.25	408,661	3,629,599	4068	4062	7
175	T17S.R09E.35	408,136	3,629,079	4044	4054	-10
176	T17S.R09E.35	408,112	3,629,296	4038	4056	-18
177	T17S.R10E.29	411,827	3,628,738	4044	4055	-11
178	T17S.R09E.36	409,274	3,628,360	4038	4050	-12
179	WHITE SANDS	389,215	3,628,257	3987	3965	22
180	T17S.R09E.35	408,127	3,628,033	4031	4043	-12
181	T17S.R09E.35	406,906	3,628,290	4021	4040	-19
182	T18S.R09E.1	409,683	3,627,525	4057	4042	15
183	T18S.R09E.1	409,735	3,627,555	4054	4042	12
184	T17S.R09E.35	406,698	3,628,292	4021	4039	-18
185	T18S.R07E.1	390,039	3,627,508	3983	3965	18
186	T18S.R08E.5	392,895	3,626,923	4020	3976	44
187	T17S.R10E.31	410,461	3,627,241	4043	4040	3
188	T18S.R07E.1	389,405	3,626,592	3991	3961	30

**TABLE 4
OBSERVED AND COMPUTED STEADY STATE WATER ELEVATIONS**

ID#	T.R.S	UTM X	UTM Y	Observed (ft msl)	Computed (ft msl)	Residual (ft)
189	T18S.R09E.1	408,398	3,626,428	4025	4030	-5
190	T18S.R10E.5	412,530	3,625,898	4032	4029	4
191	T18S.R09E.1	409,852	3,626,137	4027	4030	-3
192	T18S.R08E.12	398,507	3,626,094	4011	3994	17
193	T18S.R10E.6	411,154	3,626,157	4041	4031	10
194	T18S.R09E.11	407,346	3,625,237	3985	4018	-33
195	T18S.R09E.10	406,649	3,625,829	4067	4019	48
196	T18S.R10E.7	411,272	3,624,832	4060	4022	38
197	T18S.R09E.12	408,386	3,625,227	4007	4021	-14
198	T18S.R09E.14	407,313	3,624,437	3985	4012	-27
199	T18S.R07E.14	387,971	3,623,990	3949	3951	-2
200	T18S.R09E.10	406,351	3,624,600	3996	4010	-14
201	T18S.R09E.10	406,457	3,624,783	3971	4011	-40
202	T18S.R09E.14	407,488	3,623,727	3994	4008	-14
203	T18S.R09E.13	409,123	3,623,188	4000	4009	-9
204	T18S.R10E.18	411,390	3,623,414	4021	4013	8
205	T18S.R09E.14	407,351	3,622,958	3958	4004	-46
206	T18S.R10E.21	413,326	3,621,672	4043	4005	38
207	T18S.R09E.25	409,703	3,621,150	4011	4000	11
208	T18S.R09E.26	406,941	3,620,960	3942	3992	-50
209	T18S.R07E.25	389,359	3,620,155	3954	3943	11
210	T18S.R09E.26	406,754	3,620,345	3988	3989	-1
211	T18S.R09E.34	406,096	3,619,551	3981	3983	-2
212	T18S.R10E.31	411,119	3,619,321	3991	3996	-5
213	T19S.R09E.1	408,294	3,617,990	3986	3986	0
214	T19S.R10E.4	413,083	3,617,701	3977	3995	-18
215	T18S.R10E.32	413,031	3,617,733	3987	3995	-8
216	T18S.R10E.31	410,220	3,617,943	3967	3991	-24
217	T19S.R09E.1	408,371	3,617,898	3946	3986	-40
218	T18S.R10E.33	414,099	3,617,784	4006	3995	11
219	T19S.R10E.10	414,723	3,614,546	3994	3992	2
220	T19S.R10E.17	412,344	3,613,642	3895	3989	-94
221	T19S.R09E.34	405,053	3,608,474	3843	3967	-124
222	T19S.R09E.34	405,396	3,608,994	3853	3968	-115
223	T19S.R10E.32	411,392	3,609,093	3955	3985	-30
224	T21S.R09E.2	407,430	3,597,827	3921	3971	-50

TABLE 5
STEADY STATE MODEL COMPARISON
AND STATISTICAL INFORMATION

STEADY STATE	2005 MODEL	1-T MODEL	1989 MODEL
Residual Mean	-5.6	-17.7	-18.1
Res. Std. Dev.	27	45	39
Sum of Squares	1.7E+05	5.2E+05	3.9E+05
Abs. Res. Mean	20.1	32.8	30.8
Min. Residual	-124	-180	-206
Max. Residual	123	123	84
Range	787	787	591
Std/Range	0.035	0.057	0.065

**TABLE 6
SIMULATED WATER BALANCE
FOR JUNE 2005**

<u>IN:</u>	AFY
MOUNTAIN FRONT RECHARGE	11,890
STORAGE (FROM DRAWDOWN)	14,642
SUM	26,532
<u>OUT:</u>	
EVAPORATION	9,905
STORAGE (FROM MOUNDING)	135
PUMPING	16,491
SUM	26,532

**TABLE 7
TRANSIENT MODEL COMPARISON
AND STATISTICAL INFORMATION**

TRANSIENT	2005 MODEL	1-T MODEL	1989 MODEL
Residual Mean	5.4	-9.9	10.0
Res. Std. Dev.	31	49	43
Sum of Squares	2.0E+06	5.3E+06	4.1E+06
Abs. Res. Mean	21.7	35.1	32.7
Min. Residual	-228	-289	-247
Max. Residual	144	189	151
Range	795	795	636
Std/Range	0.038	0.062	0.068